NAVAL AIR TEST CENTER PATUXENT RIVER MD

THE NUMERICAL ANALYSIS OF AIR COMBAT ENGAGEMENTS DOMINATED BY M--ETC(U)

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Technical Memorandum

THE NUMERICAL ANALYSIS OF
AIR COMBAT ENGAGEMENTS
DOMINATED BY MANEUVERING PERFORMANCE

by

Mr. W. R. Simpson Strike Aircraft Test Directorate

and

Dr. R. A. Oberle The Center for Naval Analyses Arlington, Virginia 22209

20 June 1977



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NAVAL AIR TEST CENTER
PATUXENT RIVER, MARYLAND

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SECURITY CLASSIFICATION OF THIS PAGE(When Date Entered)

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Weapons Center (Code 4072), the Air Combat Maneuvering Range (via COMFITAEWWINGPAC), and the Center for Naval Analyses.

PREFACE

Recent emphasis on Air Combat Maneuvering (ACM), including the congressionally directed AIMVAL/ACEVAL trials, has created interest in developing methods of analysis to assess aircraft capabilities, pilot proficiency, force requirements, etc. Several methods are in use by industry, but many emphasize specific aircraft characteristics and are therefore limited in their application. This report describes an ACM analysis method developed by Mr. W. S. Stewart (Naval Weapons Center), Analyses), and Mr. W. R. Simpson (Center for Naval Dr. R. A. Oberle (NAVAIRTESTCEN). Several aspects of these analysis methods are being explored jointly by the Navy Fighter Weapons School, the Naval Weapons Center, the Center for Naval Analyses, and NAVAIRTESTCEN. These analysis techniques have been implemented at NAVAIRTESTCEN, the Naval Weapons Center, the Air Combat Maneuvering Range, and the Center for Naval Analyses. The NAVAIRTESTCEN participation was funded by the Joint Technical Coordinating Group/Munitions Effectiveness chaired by the Army Materiel Systems Analysis Agency, Aberdeen, Maryland. Assistance in the application of these techniques to specific problems of air combat is available through:

- a. NAVAIRTESTCEN (SA43)
- b. NAVWPNCEN (Code 4072)
- c. Naval Air Combat Maneuvering Range (CNA Rep to COMFITAEW-WINGPAC)
- d. Center for Naval Analyses

DECEMBER 1977

NEWENTED

J. H. FOXGROVER, RADM, USN Commander, Naval Air Test Center

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INTRODUCTION

BACKGROUND

1. The development of adequate analysis techniques in the area of Air Combat Maneuvering (ACM) is vital to the definition of the mission effectiveness of fighter aircraft, performance devices installed on fighter aircraft, and aircraft weapon systems. For the most part, however, the development of ACM testing and analysis procedures has lagged other evaluation areas such as air-to-ground or aircraft performance and flying qualities testing. Beginning in late 1971, the Commander, Operational Test and Evaluation Force initiated development of stochastic ACM analysis techniques. This effort resulted in the finite state maneuver conversion model (reference 1) and its application to the ACM evaluation of a thrust vectored attack aircraft as part of CNO Project P/V-2 (reference 2). An additional application of the maneuver conversion model to an in-flight ACM evaluation was made at NAVAIRTESTCEN for the F-11A thrust vector control system (reference 3). Following these applications, the finite state maneuver conversion model was extended by the introduction of a continuous time/continuous state performance index (reference 4). The performance index scales the offensive value of the interaircraft dynamics via the product of angle, range, and energy penalty Numerical analysis of the stochastic process resulting from the application of these two evaluation techniques to sample ACM engagements has been an ongoing effort at NAVAIRTESTCEN, NAVWPNCEN, COMFITAEW-WINGPAC and CNA. The goal of the exploitation has been the development of tactically meaningful readiness measures through further mathematical development of the ACM models for application in aircraft test and evaluation and pilot training.

PURPOSE

- 2. This memorandum is intended as a supplement to references 1 and 4 to discuss the implementation of ACM analysis methods at several facilities, to present further developments, and to illustrate the use of the analytical methods via application to an example data set selected from a family of flight tests conducted on the Air Combat Maneuvering Range (ACMR). The data base and the numerical techniques described are also being used to guide further investigations into stochastic models useful for evaluating air combat maneuvering engagements.
- 1) R. A. Oberle, Air Combat Maneuver Conversion Model, Center for Naval Analyses Report No. CRC274, of Nov 1974.
- 2) Final Report, CNO Project P/V-2 (Battle Cry) (Task XII), Commander, Operational Test and Evaluation Force, Conduct an Operational Appraisal of the AV-8A Aircraft, of 24 Apr 1974 (Secret Report).
- 3) W. R. Simpson and M. T. Pilletere, Navy Evaluation of F-11A Inflight Thrust Control System, NAVAIRTESTCEN Report SA-C3R-76, Confidential Supplement to NAVAIRTESTCEN Report SA-75R-75, of 26 Jan 1976.
- 4) W. R. Simpson, <u>Development of a Time-Variant Figure-of-Merit for Use in Analysis of Air Combat Maneuvering Engagements</u>, NAVAIRTESTCEN Technical Memorandum TM-76-1SA, of 16 Jul 1976.

METHOD OF TESTS

3. Test methods for ACM evaluation are detailed in reference 4. This memorandum addresses the form of numerical techniques applied to quantitative ACM data.

ANALYSIS PARAMETERS

4. The primary ACM parameters to be used in this memorandum are given in table I. A complete listing of general technical terms is presented at the end of this report.

Table I

ACM Parameters

Parameter Parameter	Definition		
Airplan	e Parameters		
Angle of Attack (AOA)	Angle between the free stream flow and the airplane reference line		
Normal Acceleration (N _Z)	The load factor taken perpendicular to the flight path		
Altitude (ALT)	Geometric altitude above ground level		
Indicated Airspeed (IAS)	Airspeed measured by AIS uncorrected for position error		
Specific Energy (E _S)	Sum of the weight specific kinetic and potential energies		
Target Mach Number (MT)	Mach number of the target airplane		

Interairplane Parameters

Range (R)	Line of sight distance between the c.g. of two airplanes
Closing Velocity (VC)	Time rate of change of range
Antenna Train Angle (ATA)	The angle between the aircraft reference line forward of the c.g. and any sight line
Angle Off Tail (AOT)	The angle between the aircraft reference line aft of the c.g. and any sight line

Table I (Cont'd)

Parameter	Definition		
Aı	nalysis Parameters		
Performance Index	A time variant figure-of-merit based on angular, range and energy penalty functions (detailed in reference 4)		
Conversion Coefficient	An ACM state adaptation of the per- formance index (detailed in this mem- orandum)		
ACM State	Maneuver conversion model state (detailed in reference 1)		

ANALYSIS METHODS

The primary analysis methods employed in this report are the maneuver conversion model (detailed in reference 1) and the performance index model (reference 4). The maneuver conversion model characterizes an ACM engagement as a realization of a semi-Markov process with state conversion probabilities and time in state distributions. The performance index model is a continuous state continuous time stochastic process. A secondary analysis method, the conversion coefficient, combines the continuously varying measurement of the performance index and the state definitions of the maneuver conversion model to yield a third continuous time process. This third model, although suffering from discontinuities at state boundaries, is also being investigated for applicability to ACM evaluation. These models are used in combination because of their complimentary nature and the fact that the same conclusions follow from the three methodologies. Even though the maneuver conversion model includes a no-history Markov assumption and the performance index and conversion coefficient models assume a continuous time dependence, no conflict between results has yet been observed, nor is any expected. It is anticipated that for field application the analysts can select any of the methodologies for planning and evaluating a group of ACM flight tests. The methodology will primarily be chosen on the basis of off-line computational capability as well as the mathematical sophistication of the intended data usage.

ANALYSIS PROGRAMS

GENERAL

6. An analysis capability has been developed to define pertinent information and identify significant conclusions for air combat maneuvering engagements up to four fighter aircraft versus four target aircraft. Computer programs are available which calculate analysis data for specific aircraft pairs, fighter or bogie section analysis data for two-on-one engagements, and a stochastic analysis program for two-on-one engagements which is extendable to many versus many. The primary modes of analysis in these programs are the characterization of the semi-Markov parameters of the maneuver conversion model and a one dimensional evaluation of the stochastic process during the performance index model, together with stochastic data for the conversion coefficient and an expression of the expected paths for a statistical sample. The resulting numerical techniques are being used by the authors to support further theoretical development. For example, in reference 4, a feedback sequence leading to the development of a predictor model is discussed. Achievement of this predictor model requires a theoretical characterization of the underlying probability space for which the performance index and conversion coefficient are natural realizations. Identification of this underlying probabilistic structure is the goal of the ongoing investigations.

PAIRED ANALYSIS

7. The first step in the analysis is the computation of analysis parameters for fighter-to-adversary pairs in the engagement. The NAVAIRTESTCEN implementation of the paired analysis computer program is given in appendix A. Input is taken as the aircraft and interaircraft data of table I. These data are directly available from tests conducted at the ACMR in Yuma, Arizona, but can also be computed from use of radar data and onboard tape. Required inputs to the program are given in table II. These inputs are assumed to be at 1 second intervals from initialization. The beginning of the engagement can be taken analytically (such as at first visual contact) or mathematically (such as a fixed interaircraft range). Because of the inconsistency of results initialized at first visual contact, the latter is recommended.

Table II Input Required for Paired Analysis Program

Input Definition				
TITLE	A 50-character identifier of the engagement			
ES1	Fighter aircraft specific energy	(1)		
ES2	Target aircraft specific energy			
AOT	Fighter-to-target angle off tail			
ATA	Fighter-to-target antenna train angle			
R	Fighter-to-target interaircraft range			
RMAX1	Fighter offensive maximum range	(2)		
RMAX2	Fighter defensive maximum range			
ROPTI	Fighter optimum missile launch range			
ROPT2	Target optimum missile launch range			
RO1	Target zero penalty range			
ROZ	Fighter zero penalty range			
RG1	Fighter range at which guns tactics begin to dominate fight			
RGZ	Target range at which guns tactics begin to dominate fight			
EDEV1	Fighter energy relevance term			
EDEV2	Target energy relevance term			
FG1	Fighter interenvelope gun penalty			
FG2	Target interenvelope gun penalty			
ATAOF	Antenna train angle for offensive state	(3)		
AOTOF	Angle off tail for offensive state			
ATAWEP	Antenna train angle for weapons envelope			
AOTWEP	Angle off tail for weapons envelope			
RIWEP	Weapons envelope minimum range			
R2WEP	Weapons envelope maximum range			
RNUT				
NFILES	The number of data files to be input			
PRINT	Print Option 1 for terminal output 5 for printer output	etta xel		
GRAF	Graph Option 1 for terminal output 5 for printer output			

NOTES: (1) As a function of time (2) Defined in reference 4 (3) Defined in reference 1

8. The program computes and graphs the paired analysis data. An example data run is given in appendix B. Data output is defined in table III, and output data are placed on disk file for further use.

Table III
Output From Paired Analysis Program

Output	Definition	Notes
TIME	Assumed 1 second interval beginning at 1	
RANGE	Interaircraft range from table II	(1)
AOT	Angle off tail from table II	
ATA	Antenna Train Angle from table II	
NRG #1	Fighter aircraft ES1 from table II	
NRG #2	Target aircraft ES2 from table II	
DIR ANG	Normalized Directional Angle	(2)
NRG FN	Energy function for performance index calculation	
RNG FN	Range function for performance index calculation	
PERF INDEX	Performance Index	
STATE	ACM State	(3)

NOTES: (1) Output only on printer (print option 5). Not included in appendix B output.

- (2) Defined in reference 4.
- (3) Defined in reference 1.

SECTION ANALYSIS

9. The section coefficient data are computed by a second program as given in appendix C. The program was written for two versus one engagements and requires two output files generated by the previous program. These output files are for the two fighter-to-target pairs. The program computes the section performance index, section coordination, coordination consistency, the conversion coefficient, and the ACM state by the two-on-one state definitions of reference 1.

Section Performance Indices

10. The section performance indices are computed by the magnitude sum method (the vector sum method of reference 4). Section coordination and coordination consistency are computed as per reference 4.

Conversion Coefficient

11. The conversion coefficient was introduced to compensate for difficulties arising in the tactical interpretation of the section performance index. Specifically, as more aircraft are introduced, the section performance index becomes less responsive to tactical extremes because of mathematical "washout." That is, alternate signs in the performance index cancel to yield a numerically neutral fight which is often not representative of the tactical situation. For example, a precise interpretation of the "daisy chain" shown in figure 1 cannot be realized mathematically. The individual fighter-to-target performance indices cancel mathematically, yet tactically the fighter section is advantaged.



Figure 1
Air Combat "Daisy Chain" for Two-On-One Engagements

- 12. The situation as shown in figure 1 favors the fighter section if none of the aircraft are in a weapons envelope because of two very important reasons:
 - a. The forward fighter has a friendly observer looking over his rear quarter (the rear fighter).
 - b. In an attempt to close to the weapons envelope, the target aircraft in the middle will be flying a flight path which is in a large part determined by the first aircraft whose maneuvers can be made known to the rear aircraft. The situation will last only a short time with a smart pilot in the center aircraft and will quickly lead to "bogie switching," (a term applied to the situation) where the target (center) aircraft switches his offensive press to the other fighter.

13. The extension of the maneuver conversion model given in table IV covers this point adequately. (Rule 2 applies to the "daisy chain" of figure 1.)

Table IV(1)

Rules for State Evaluation of a Two-On-One Engagement

- 1. The section is OFFENSIVE WEAPON when at least one member is in offensive weapon state and the other is higher than a fatal defensive state.
- 2. The section is OFFENSIVE when at least one member has an offensive position and the other is higher than a fatal defensive state.
- 3. The section is NEUTRAL when both members are in neutral state.
- 4. The section is DEFENSIVE when at least one member is in defensive state and the other is either neutral or defensive.
- 5. The section is FATAL DEFENSIVE when at least one member is in fatal defensive state and the other has less than offensive weapon state.
- 6. The section is in a TRADE OFF state when one member of the section is in offensive weapon state and the other is in a fatal defensive state.

NOTE: (1) Taken from reference 1.

- 14. The conversion coefficient introduced in this memorandum is an attempt to modify the performance index to cover the "daisy chain" situation and increase responsiveness. It is computed along the lines of table IV as follows:
 - a. The conversion coefficient is equal to the section performance index when both of the paired performance indices are less than 30 in absolute value (corresponding to conditions 3 and 4 of table IV).
 - b. The conversion coefficient is equal to the section performance index when both paired performance indices have the same sign (corresponding in part to conditions, 2, 3, and 4 of table IV).
 - c. The conversion coefficient is equal to the section performance index when the paired performance indices are both greater than 75 in absolute value and opposite in sign (corresponding to condition 6 of table IV). These are flagged as a trade-off situation.

d. The conversion coefficient is not equal to the section performance index when the paired performance indices are opposite in sign and one is greater than 30 but less than 75. In this case, the conversion coefficient is computed as follows:

CONCO =
$$PI_1^2 \left(1 - \frac{|PI_2|}{75}\right)$$
 (1)

where PI₁ is the positive value of the paired performance indices. This weights the positive (offensive factor) but degrades to a neutral value as a defensive fatal situation evolves (corresponding to condition 2 of table IV).

e. The conversion coefficient is not equal to the section performance index when the paired performance indices are opposite in sign with one greater than 75 in absolute value and both greater than 30 in absolute value. In this case, it is computed as follows:

CONCO =
$$PI_1^2 \left(1 - \frac{|PI_2|}{400}\right) \left(\frac{|PI_1|}{PI_1}\right)$$
 (2)

where PI₁ is the paired performance index greater than 75 in absolute value and PI₂ is the other paired performance index. This weights the offensive weapons and defensive fatal states (corresponding to conditions 1 and 5 of table IV).

15. The conversion coefficient combines the best features of the maneuver conversion model with the performance index model but suffers in discontinuities due to equation changes at specified points. Care must be taken in further extensions of the conversion coefficient to include not only the case of the "daisy chain" (figure 2 shows a two versus two "daisy chain") but also other potential situations which cannot readily be described functionally such as the "floating diamond" in figure 3.

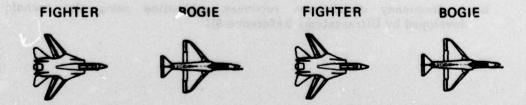


Figure 2
Air Combat "Daisy Chain" for Two-On-Two Engagements

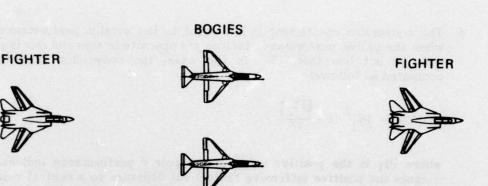


Figure 3
Air Combat "Floating Diamond" for Two-On-Two Engagements

Maneuver Conversion Model

16. The computation of the two-on-one ACM state is taken directly from table IV as obtained from reference 1.

Output of Section Analysis Program

17. An example output of the section analysis program is given in appendix D. The data are self-explanatory. These data are additionally output onto disk for use in the stochastic analysis program.

STOCHASTIC ANALYSIS

- 18. The stochastic analysis program takes the output data from both previous programs for a large sample of data. Because of the number of data points and calculations required, the program requires segmentation to fit most computers (the program given in appendix E takes in excess of 250K storage). Pertinent features of the program are:
 - a. A file of data management options which allows the user to selectively compute and output data as documented in appendix E.
 - b. A frequency distribution recovery subroutine using the techniques developed by Ultrasystems (reference 5).
- 5) Dr. R. Curry and Dr. R. Egbert, <u>Investigation of Distribution Recovery Techniques</u>, Operations Research and Economic Analysis Development Department, <u>Ultrasystems</u>, Incorporated, Newport Beach, California, 11 Feb 1974.

- c. A moment generating routine calculating the classical moments of distributed functions with a given frequency distribution (reference 6).
- d. An integration routine for integration of equally spaced functions using a combination of Simpson's rule and Newton's three-eighths rule (reference 7).
- e. A general plot routine for use of the line printer in plotting developed at the NAVAIRTESTCEN.
- 19. The purposes of the stochastic analysis program are to:
 - a. Compute the frequency distributions of the continuous variables in time for section data and paired data.
 - b. Compute the first 4 moments of these frequency distributions.
 - c. Compute the maneuver conversion/conversion probability matrix for aircraft sections and pairs.
 - d. Compute the time in state frequency distributions for the maneuver conversion model.
 - e. Compute the first 4 moments of these frequency distributions.

Stochastic Analysis Program Output

20. Full output of the stochastic analysis program is too voluminous to present here. Selected output for the test run and significant analysis information is, however, included for documentation. The test run, while representing actual engagement data, is for purposes of illustrating analysis methodology only. Separate reports are being written covering test data analysis and conclusions.

Continuous Variable Frequency Distributions and Moment Data

- 21. Frequency data output at 5 second intervals and for selected values of the performance index are shown in table V for a sample data set. The conclusions to be drawn from the data set are a function of the frequency value assumed to be significant. For example, the attainment of an optimal position (either best or worst) will come much less frequently than the neutral position. In table V, if a significance level of .001 is used, it can be seen that an optimal position will be attainable for the fighter section 20-30 seconds into the fight (a performance index of +100). This value does not occur until 80-90 seconds for the target (a performance index value of -100). This would indicate an early advantage to the fighter section and a recommended action to press and exploit the early advantage.
- 6) H. G. Kendall, The Advanced Theory of Statistics, Vol. I. Hafner Publishing Company, New York, 1958.
- 7) System 360 Scientific Subroutine Package (360A-CM-03X) Version II Programmers Manual, International Business Machines Report H20-0205-2, White Plains, N.Y., 1967.

Table V

Performance Index Distribution for Two-On-One Example Data Set

			-		The second secon			The second secon	The same of the sa	
Time	-100	-98	-80	-78	0	2	80	82	86	100
(sec)					Frequency	cy Index				
1	0.00000	0.00000	0.00000	0.00000	0.03268	0.03643	0.00000	0.00000	0.00000	0.00000
9	0.00000	0.00000	0.00001	0.00001	0.01432	0.01553	0.00004	0.00002	0.00000	0.00000
=	0.00010	0.00012	0.00044	0.00050	0.00944	92600.0	0.00157	0.00135	0.00030	0.00025
16	0.00025	0.00029	0.00092	0.00103	0.00793	0.00814	0.00273	0.00246	0.00092	0.00080
17	0.00061	0.00068	0.00149	0.00160	0.00805	0.00819	0.00303	0.00280	0.00132	0.00119
92	0.00058	0.00064	0.00135	0.00146	90800.0	0.00822	0.00323	0.00299	0.00148	0.00134
31	0.00016	0.00019	0.00076	0.00087	0.00949	0.00953	0.00232	0.00212	0.00000	0.00080
36	0.00032	0.00036	0.00100	0.00111	0.00955	0.00963	0.00228	0.00209	0.00093	0.00082
41	0.00010	0.00012	0.00040	0.00044	0.01115	0.01133	0.00177	0.00155	0.00043	0.00035
46	0.00011	0.00013	0.00047	0.00053	0.01055	0.01073	0.00173	0.00153	0.00047	0.00039
51	0.00000	0.00000	0.00011	0.00015	0.01245	0.01263	0.00019	0.00014	0.00001	0.00001
26	0.00000	0.00000	0.00010	0.00014	0.01238	0.01237	0.00028	0.00021	0.00002	0.00001
5	0.00003	0.00004	0.00030	0.00036	0.01229	0.01228	0.00078	99000.0	0.00013	0.00010
3	0.00009	0.00011	09000.0	0.00000	0.01064	0.01068	0.00132	0.00116	0.00034	0.00029
=	0.00043	0.00049	0.00129	0.00142	0.00858	0.00867	0.00262	0.00241	0.00109	0.00097
20	0.00054	0.00061	0.00155	0.00169	0.00809	0.00814	0.00287	0.00266	0.00132	0.00120
8	0.00057	0.00065	0.00178	0.00195	0.00799	0.00808	0.00220	0.00199	0.00080	0.00070
86	0.00150	0.00161	0.00287	0.00302	96900.0	0.00697	0.00328	0.00311	0.00187	0.00173
5	0.00173	0.00185	0.00308	0.00323	0.00734	0.00734	0.00282	0.00268	0.00169	0.00159
96	0.00093	0.00104	0.00254	0.00276	0.00850	0.00839	0.00158	0.00147	0.00074	0.00068
101	0.00125	0.00138	0.00300	0.00323	0.00805	0.00794	0.00166	0.00154	0.00078	0.00071
106	0.00057	0.00066	0.00215	0.00240	0.00835	0.00820	0.00126	0.00113	0.00041	0.00035
Ξ	0.00067	0.00077	0.00212	0.00232	0.00791	0.00793	0.00173	0.00155	0.00054	0.00047
116	0.00124	0.00137	0.00288	0.00309	0.00110	0.00765	0.00200	0.00185	0.00089	0.00081
121	0.00057	0.00067	0.00243	0.00272	0.00820	0.00809	0.00081	0.00071	0.00022	0.00018
126	0.00089	0.00100	0.00255	0.00278	0.00810	0.00803	0.00153	0.00139	0.00056	0.00049
131	0.00100	0.00112	0.00253	0.00273	0.00788	0.00785	0.00206	0.00190	0.00089	0.00080
136	0.00103	0.00114	0.00247	99200.0	0.00798	96200.0	0.00224	0.00209	0.00105	9600000
141	98000.0	96000.0	0.00229	0.00249	90800.0	0.00799	0.00229	0.00214	0.00115	0.00106
146	0.00130	0.00142	0.00285	0.00305	0.00768	0.00762	0.00236	0.00222	0.00124	0.00114
151	99000.0	0.00076	0.00216	0.00239	0.00845	0.00827	0.00189	0.00177	0.00093	0.00085
156	0.00121	0.00134	0.00292	0.00314	0.00810	96200.0	0.00197	0.00188	0.00121	0.00114
161	0.00129	0.00142	0.00306	0.00328	0.00804	0.00790	0.00172	0.00162	0.00088	0.00080
166	0.00185	0.00201	0.00374	0.00396	0.00699	0.00686	0.00237	0.00226	0.00145	0.00136
171	0.00276	0.00291	0.00442	0.00459	0.00674	0.00665	0.00243	0.00234	0.00169	0.00162
176	0.00256	0.00273	0.00448	0.00469	86900.0	0.00685	0.00192	0.00184	0.00130	0.00124
181	0.00343	0.00357	0.00487	0.00502	0.00660	0.00651	0.00233	0.00225	0.00167	0.00161
186	0.00089	0.00102	0.00284	0.00313	0.00839	0.00812	0.00073	0.00065	0.00022	0.00019
				The second name of the last of		The state of the s	A STANSANTON OF THE PERSON OF	THE CONTRACTOR DESIGNATION OF THE PERSON NAMED IN COLUMN TWO PERSONS NAMED IN COLUMN TRACTOR NAMED IN COLUMN TWO PERSONS NAMED IN COLUMN TRACTOR NAMED		

- 22. For the fringe of a weapons envelope (as shown in table V) at a value of +80 for the fighter or -80 for the target, a significance level of .003 may be chosen due to the higher incidence of occurrence. These values again occur at 20-30 seconds for the fighter section (+80 performance index) and much later, 80-90 seconds for the target (-80 performance index) with the same conclusions. Further, the data indicate a loss of this advantage in the later stages of the fight due to the higher frequency of occurrence of performance indices in the negative range after 90 seconds, suggesting it may be desirable for the fighters to stay engaged for only short periods (say up to 60 seconds). The defensive disengagement for the fighter section between 60 and 90 seconds is the tactical defense to the tide of battle shifting to the bogie. The neutral values (values of performance index near 0) are included for reference.
- 23. Table VI shows the statistical summary data for the data of table V. The variation of the mean as a function of time points again to an early advantage to the fighter section and loss of that advantage at around 90 seconds into the fight. The variance shows that events in the latter half of the engagement are more random in nature (larger relative values of variance). That is, events are less in control of either the fighter section or the target section, but not a significant difference. The value of the mean is indicative of the relative worth of the two sections and the engagements show to be predominantly neutral with a slight advantage to the fighter section initially and a slight advantage to the target section later in time. The overall conclusion is that the sections are fairly equally matched. The third and fourth moments were computed for later analysis and model building.
- 24. Figure 4 shows the output of the frequency of occurrence plot as a function of performance index for the start of the set of engagements. Figure 4(a) shows a tightly distributed data set in the region of -16 to +20 indicating a neutral start condition. One or more engagements are seen to start with the fighter section at a disadvantage as shown in the secondary peak between -30 and -16, and these engagements should probably be deleted from the engagement set for the neutral start analysis.

Table VI
Summary Statistics for Section Performance Index Distribution

Time (sec)	Number of Points	Mean Performance Index	Variance of Performance Index	Third Moment of Performance Index About Mean	Fourth Moment of Performance Index About Mean
1	33	6.34	114.37	-636.67	56159.57
6	33	12.80	462.40	-4176.03	757210.59
11	33	14.57	1151.75	-12832.23	3800686.85
16	33	13.90	1570.17	-19020.63	6318563.84
21	33	10.42	1811.55	-17839.51	8065442.44
26	33	12.29	1782.15	-19620.96	7975665.77
31	33	8.27	1491.78	-1178.67	5558583.45
36	33	8.14	1527.16	-5578.23	6023055.01
41	33	13.02	1120.23	-4447.80	3593418.53
46	33	11.47	1198.91	-5504.27	3974260.30
51	32	5.99	807.96	-4006.78	1734312.40
56	32	3.55	847.04	380.94	1840745.63
61	32	4.27	1000.48	1595.19	2757920.97
66	32	4.97	1249.15	-201.43	4090099.35
71	30	8.30	1702.58	-9678.55	7107357.44
76	30	7.00	1850.01	-7680.61	8024471.00
. 81	30	4.25	1800.18	-9594.28	7555697.28
86	30	2.31	2300.12	-5018.21	11336444.27
91	29	-0.77	2242.77	1069.86	11057383.18
96	28	-7.02	1766.26	12959.65	7677819.65
101	27	-8.54	1871.21	15561.02	8432997.65
106	27	-8.12	1624.86	14356.95	6497451.97
111	27	-0.96	1797.02	-1663.24	7357124.42
116	27	-4.89	1983.82	8765.20	8980127.66
121	27	-11.43	1540.44	12607.21	5774302.76
126	25	-6.31	1789.32	9495.46	7541745.63
131	24	-2.79	1934.10	5310.66	8574531.13
136	24	-1.51	1957.46	3766.21	8824056.90
141	21	-1.93	1927.95	9173.04	8660194.07
146	19	-3.53	2064.53	9781.27	9692787.76
151	19	-6.13	1768.54	19825.28	7818620.14
156	18	-7.86	1930.58	21118.76	9156490.34
161	18	-9.46	1879.12	19982.05	8677585.29
166	16	-9.20	2209.73	27797.15	11175677.66
171	14	-10.19	2369.51	27960.52	12478168.37
176	14	-13.59	2179.04	31991.96	11230738.18
181	12	-11.99	2422.24	30528.05	12983093.75
186	10	-16.13	1456.25	18236.56	5761935.46

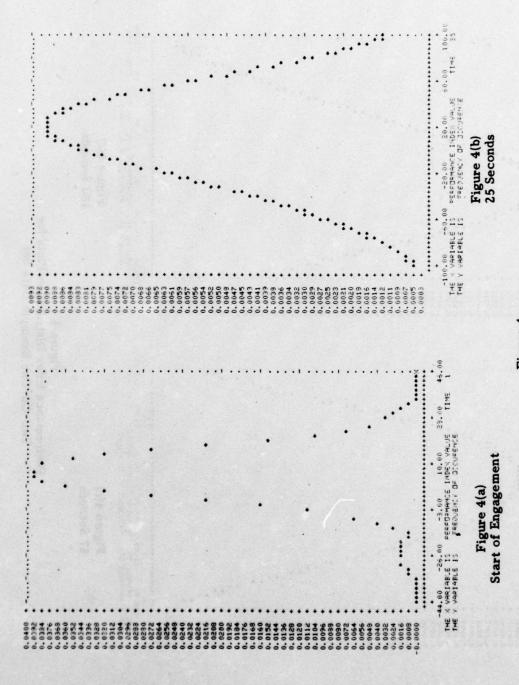


Figure 4
Performance Index Distribution Plots for
Two-On-One Example Data Set

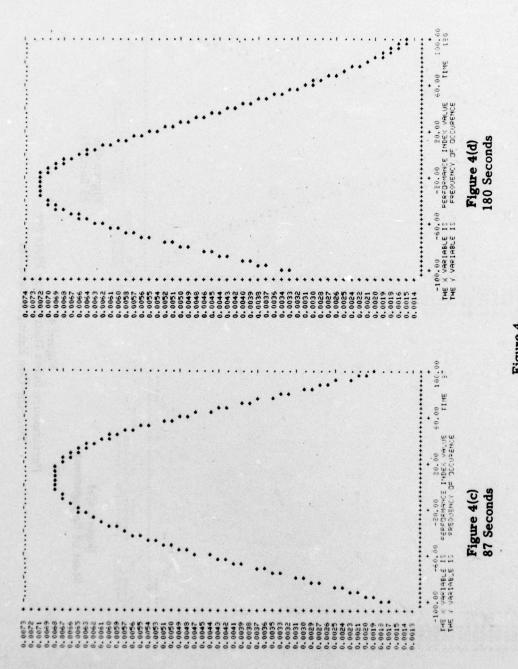
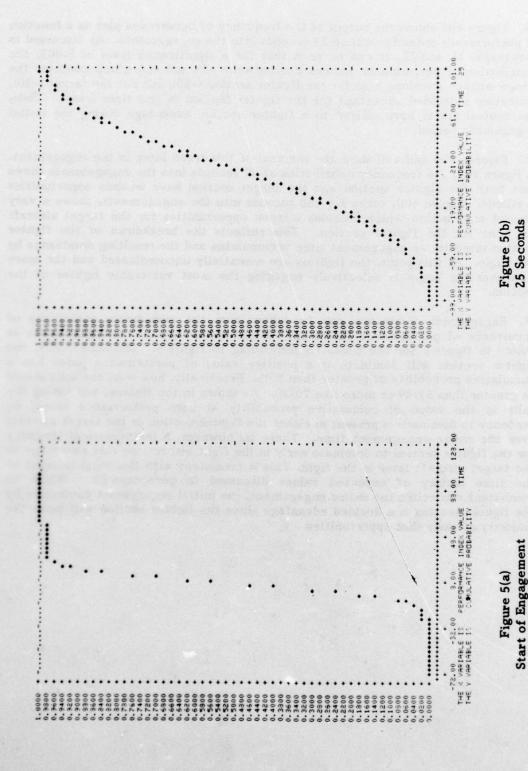


Figure 4
Performance Index Distribution Plots for Two-On-One Example Data Set

- 25. Figure 4(b) shows the output of the frequency of occurrence plot as a function of performance index for a time 25 seconds into the engagements. As discussed in paragraphs 21 and 22, it can be seen that for a significance level of 0.003, the distribution of performance indices lies between -54 and +82 which contains the fringe weapon envelope case for the fighter section (+80), but not the target (-80), indicating a decided advantage for the fighter section in this time frame. Thus, the neutral starts have shifted to a fighter section advantage during the initial engagement period.
- 26. Figures 4(c) and 4(d) show the reversal of this trend later in the engagement. In figure 4(c), the frequency distribution at 87 seconds into the engagements shows that both the fighter section and the target section have weapon opportunities available. Figure 4(d), taken for 180 seconds into the engagements, shows a very skewed distribution which includes weapon opportunities for the target aircraft but none for the fighter section. This reflects the breakdown of the fighter section integrity as engagement time accumulates and the resulting dominance by the bogie. At this point, the fighters are essentially uncoordinated and the more maneuverable bogie is selectively engaging the most vulnerable fighter of the section.
- 27. Engagement dominance can be taken from the cumulative probability of occurrence of performance indices at various times during the engagements as shown in figure 5 for the times corresponding to figure 4. Mathematically, the fighter section will dominate if a positive value of performance index has a cumulative probability of greater than 50%. Practically, however, the split should be greater than 51/49 or more like 70/30. As shown in the figures, and taking the split in the value of cumulative probability at zero performance index, no tendency to dominate is present in either the fighter section or the target aircraft over the entire engagement time. There is, however, a mathematical tendency for the fighter section to dominate early in the fight and to lose this advantage to the target aircraft later in the fight. This is consistent with the trend isolated by the time history of expected values discussed in paragraph 23. While no combatant controlled the entire engagement, the initial engagement dominance by the fighter section is a decided advantage since the fighter section will incur the majority of early shot opportunities.



Start of Engagement

Figure 5 Cumulative Probability Plots for Performance Indices of Two-On-One Example Data Set

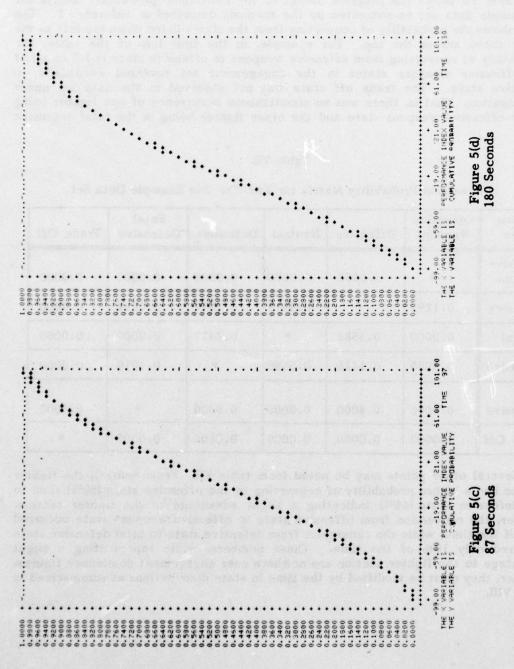


Figure 5
Cumulative Probability Plots for Performance Indices
of Two-On-One Example Data Set

Maneuver Conversion/Conversion Probability Matrix

28. Table VII shows the program output of the conversion probability matrix for the sample data set as computed by the methods described in reference 1. The table shows the probability of converting from the states listed down the left to the states listed across the top. For example, in the first line of the table, the probability of converting from offensive weapons to offensive state is 1.0 or all of the offensive weapons states in the engagement set reverted eventually to offensive state. The trade off state was not observed in the data set under investigation. That is, there was no simultaneous occurrence of one fighter being in the offensive weapons state and the other fighter being in the fatal defensive state.

Table VII

Conversion Probability Matrix for Two-On-One Example Data Set

Section State	Offensive Weapons	Offensive	Neutral	Defensive	Fatal Defensive	Trade Off
Offensive Weapons		1.0000	0.0000	0.0000	0.0000	0.0000
Offensive	0.1293		0.5918	0.2517	0.0272	0.0000
Neutral	0.0000	0.5583		0.4417	0.0000	0.0000
Defensive	0.0000	0.3426	0.5556	•	0.1019	0.0000
Fatal Defensive	0.0000	0.4000	0.0000	0.6000		0.0000
Trade Off	0.0000	0.0000	0.0000	0.0000	0.0000	*

29. Several other points may be noted from table VII. From neutral, the fighter section had a higher probability of converting to the offensive state (56%) than to the defensive state (44%) indicating a slight advantage to the fighter section. Further, the conversion from offensive state to offensive weapons state occurred 13% of the time, while the conversion from defensive state to fatal defensive state occurred only 10% of the time. These numbers, while representing a slight advantage to the fighter section are nowhere near engagement dominance figures. Further, they must be modified by the time in state distributions as summarized in table VIII.

Table VIII

Time in State Summary for Two-On-One Example Data Set

Section State	Number of Points	Mean Time in State (sec)	Variance of Mean Time in State (sec ²)	Third Moment about Mean Time in State (sec ³)	Fourth Moment about Mean Time in State (sec ⁴)
Offensive Weapons	18	2.93	4.39	9.74	68.59
Offensive	142	14.52	141.52	2329.60	96707.36
Neutral	153	18.13	206.64	3876.30	197143.09
Defensive	97	15.30	136.32	1862.18	77235.03
Fatal Defensive	16	2.56	5.08	14.96	96.76
Trade Off	0	0.00	0.00	0.00	0.00

- 30. As shown in table VIII, the mean time spent in the offensive state is somewhat less than the mean time spent in the defensive state for roughly the same variance (same degree of consistency), thus offsetting the partial advantage to the fighter section. The nonparametric frequency function fits for time in offensive, neutral, and defensive states displayed the log normal characteristic referred to in reference 2. Figure 6(a) shows the time in state distribution for the offensive state.
- 31. Time in state distributions for the offensive weapons and defensive fatal states are multimodal and means do not compare directly. Figure 6(b), the time in state distribution of the offensive weapons state for the fighter section, is characterized as a bimodal distribution which approximates the log normal form. Figure 6(c), the time in state distribution of the fatal defensive state for the fighter section, is characterized by a trimodal distribution which approximates the log normal form. The primary difference in the two states is probably characterized by the pilot tactics employed in two-on-one engagements. The first peak in figure 6(b) probably represents a transient or "flash through" computation in the neighborhood of one second, while the second peak (at 8.5 to 9 seconds) represents the tracking solution. The fatal defensive state (figure 6(c)) shows both these peaks, together with an intermediate peak which is probably due to 'bogie switching' as discussed in paragraph 12. The target aircraft, being threatened, in some instances would not complete the tracking solution, but hold the state for some finite time (around 5 seconds), fire a missile, and then switch. No such pressures to switch states are incumbent upon the fighter section in a two-on-one engagement. This intermediate short duration peak could be termed the 'survival sting' peak. This logic would lead to the supposition that a trimodal distribution for offensive weapons and defensive fatal states would be present in all engagements with multiple bogies and multiple fighters. The above observations are based upon a small data base and must be verified by further data samples.

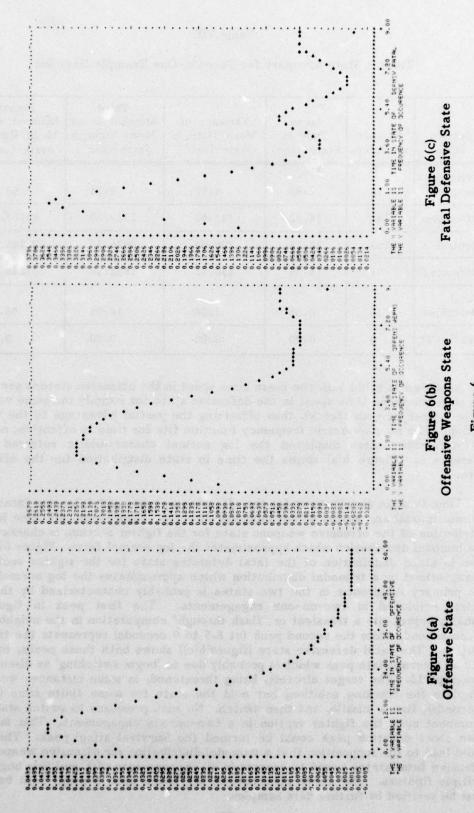


Figure 6
Time in State Distributions for Two-On-One Example Data Set

- 32. The above discussion exhausts the conclusions that can be drawn directly from the estimated values of the maneuver conversion parameters. Further analysis, for example, the complete characterization of the underlying probability space and the estimation of the expected trade off ratio (the ratio of the probability of a win to the probability of a loss), requires the methodology described in reference 8. Since the techniques are adequately described in reference 8, they will not be repeated here.
- 33. At this point in the analysis, the semi-Markov process of the maneuver conversion model is defined, and when integrated with the weapon employment parameters, the full range of ACM measures of effectiveness including exchange ratios, survivability and dominance indices, etc., can be computed. These terms are treated in detail in references 1 and 8. The stochastic process of the performance index is only partially defined and is still in the developmental phase.

MODEL VALIDATION

34. The question of model validity may be addressed at two levels. The first level is consistency of conclusions drawn from the differing analytic techniques. The above discussions demonstrate this consistency for the data set under consideration. The authors believe that the two models are equally right or equally wrong. Thus, validation is reduced to determining if either model characterizes ACM correctly. An indication of this validity has already been obtained by noting the consistency of the common conclusion set with the intuitive evaluation of the participating aircrews. A formal mathematical validation may be obtained by comparing the tactical measures (listed in reference 1) as estimated from the computer solution of the semi-Markov process and as estimated directly from the data sample. Although this has not been done for this data sample, a valid comparison has been described in reference 8.

8) R. A. Oberle and W. R. Nunn, <u>Evaluation of Air Combat Maneuvering</u> Engagements, CNA Study No. 77-3, (to be published).

CURRENT RESEARCH

35. The above discussion summarizes some of the early research into the evaluation of test range ACM engagements. Work is continuing toward the development of a completely mathematical characterization of such engagements. Specifically, the investigations are directed toward a complete characterization of the underlying probability structure for which the performance index and conversion coefficient are natural realizations. The numerical techniques discussed above not only provide tactically significant data interpretation techniques but also serve as the initial technical tools to support the ongoing research. Further numerical techniques which are expected to be useful for data interpretation include a full nonparametric covariance and increment analysis along with selected distribution fitting analyses. The current research emphasis centers around a characterization of the performance index as a solution of a stochastic differential equation. It is expected that such a characterization will identify a few stochastic parameters that will serve to replace the mass of numerical calculations currently necessary as well as identify the theoretical connection between the maneuver conversion and the performance index models.

REFERENCES

- 1. R. A. Oberle, Air Combat Maneuver Conversion Model, Center for Naval Analyses Report No. CRC274, of Nov 1974.
- Final Report, CNO Project P/V-2 (Battle Cry) (Task XII), Commander, Operational Test and Evaluation Force, Conduct an Operational Appraisal of the AV-8A Aircraft, of 24 Apr 1974 (Secret Report).
- 3. W. R. Simpson and M. T. Pilletere, Navy Evaluation of F-11A Inflight Thrust Control System, NAVAIRTESTCEN Report SA-C3R-76, Confidential Supplement to NAVAIRTESTCEN Report SA-75R-75, of 26 Jan 1976.
- 4. W. R. Simpson, Development of a Time-Variant Figure-of-Merit for Use in Analysis of Air Combat Maneuvering Engagements, NAVAIRTESTCEN Technical Memorandum TM-76-1SA, of 16 Jul 1976.
- 5. Dr. R. Curry and Dr. R. Egbert, <u>Investigation of Distribution Recovery Techniques</u>, Operations Research and Economic Analysis Development Department, Ultrasystems, Incorporated, Newport Beach, California, of 11 Feb 1974.
- 6. H. G. Kendall, The Advanced Theory of Statistics, Vol. I, Hafner Publishing Company, New York, 1958.
- 7. Systems 360 Scientific Subroutine Package (360A-CM-03X) Version II Programmers Manual, International Business Machines Report H20-0205-2, White Plains, N.Y., 1967.
- 8. R. A. Oberle and W. R. Nunn, Evaluation of Air Combat Maneuvering Engagements, CNA Study No. 77-3, (to be published).

PAIRED ANALYSIS PROGRAM

```
L PFINDX_
FILE: PFINDX -03/13/76 10:22 AM.
100 BERRMES
200 FILE 5
          5=RANDY. UNIT=PRINTER BACKUP DISK
300 FILE 4=REF.UNIT=DISK
400 FILE 2=ACM, UNIT=BISK
500 FILE 3=CNST,UNIT=D1SK
600 FILE 1=TRMNL,UNIT=REMOTE
700 INTEGER X
    REAL K
300
900
    DIMENSION TITLE (50)
910 DIMENSION ISTAT (500)
1000 DIMENSION STATE (500)
1100 DIMENSION BE(500) AA(500)
      DATA BLANK, DOT, STAR, XXXX" ", ", ", ", ", "X"/
1200
1300 DATA PLUS/"+"/
1400 DATA OFWEP, OFF, DEF, NUT, DEFAT/"W", "O", "D", "N", "F"/
1419 C-
1420 C- DATA FOR ACM STATE CALCULATION WEDFFENSIVE WEAPON STATE
1430 C-
                                         D=OFFENSIVE STATE
1440 C-
                                         N=NEUTRAL STATE
1450 C-
                                          D=DEFENSIVE STATE
                                         F=DEFENSIVE FATAL STATE
1460 C-
1470 C-
1480 C-
1500 DIMENSION R(500) , K(500) , FRNG (500) , DA (500) , PI (500)
1600
      DIMENSION EST (500)
1700 DIMENSION ES2 (500)
1800 DIMENSION AOT (500)
1900 DIMENSION ATA (500)
1950
      IFIL=1
      PRINT 433
1960
1970
      433 FORMAT (5X, "HOW MANY FILES AM I LOOKING AT")
1980
      READ(1,7) NFILES
0000
      KOUNT=1
2100
      READ (3, /) RMAX1.RMAX2.ROPT1.ROPT2.R01.R02.RG1.RG2.EDEV1.EDEV2.
2110 C-
2115 -F61, F62, ATAOF, ADTOF, RIWEP, REWEP, RNUT, ATAWEP, ADTWEP
2120 C- SEE FEXT FOR EXPLANATION OF THESE NUMBERS
2130 C-
2300 PRINT 434
2900 434 FORMAT(5%,"WHERE DO YOU WANT DATA OUT, 1=HERE, 5=PRINTER",
3000 -"OTHERS=NONE")
3100 READ(1,/) IPRINT
3200 PRINT 435
3300 435 FORMAT(5X,"WHERE DO YOU WANT A GRAPH, 1=HERE, 5=PRINTER",
3400 -"OTHERS=NONE")
3500 READ(1./) IGRAF
3510 86 CONTINUE
3512
      KOUNT=1
3515 READ(2,/) N, (R(I), I=1,N), (ES1(I), I=1,N), (ES2(I), I=1,N),
3520 - (ADT (I) + I=1+N) + (ATA (I) + I=1+N)
3530 READ(2:111) (TITLE(1):1=1:50)
      111 FORMAT (50A1)
3540
     191 CONTINUE
3550
3560
      WRITE(1:111) (TITLE(1):1=1:50)
     IF (IPRINT.EQ. 1. OR. IPRINT.EQ. 5) 60 TO 987
3500
3700 50 TO 100
```

```
3800 987 CONTINUE
3900 WRITE (IPRINT . 1003) (TITLE (I) . I=1.50)
4000 1003 FORMAT (1H1,10X,50A1)
4100 WRITE(IPRINT, 444) RMAX1, RMAX2, ROPT1, ROPT2, RO1, RO2, RG1, RG2,
4110 -SDEV1. EDEV2. FG1. FG2. ATAOF. ACTOF, ATAWEP. ACTWEP. RSWEP. RSWEP. RNUT
4200 444 FORMAT(10X, "INPUT CONSTANTS FOR THIS RUN",
4300 -10%," FIGHTER OFFENSIVE MAX RANGE",F10.1," TARGET =".F10.1,/
4500 -10%," FIGHTER OPT MISSILE RANGE ".F10.1," TARGET =".F10.1,/
4600 -10%," FIGHTER MINIMUM RANGE (SUM) ".F10.1," TARGET =".F10.1,/
4700 -10%, FIGHTER GUN ENVELOPE RMAX ",F10.1," TARGET =",F10.1,/
4300 -10%," FIGHTER ENERGY RELEVENCE ",F10.4," TARGET =",F10.4,/
4900 -10%." FIGHTER INTER-ENVELOPE PENAL", F10.4, " TARGET =", F10.4, / 4910 -10%. "OFFENSIVE ATA=", F10.1, " ADT=", F10.1, /
4920 -10X, "OFF WEP ATA=",F10.1, "AGT=",F10.1,
4925 -10%, "OFF WEP RMAX=",F10.1, "RMIN=",F10.1,/
4930 -10X, "FIGHT NUETRAL BEYOND", F10.1, " RANGE")
5000 IF (IPRINT.EQ. 1) WRITE (1,30)
5010 IF (IPRINT.EQ.5) WRITE (5,301)
5020 301 FORMAT(5X,"TIME RANGE AOT ATA NRG#1 NRG#2 DIR ANG",
5030 -" NRG FN RNG FN PERF INDEX STATE")
5100 30 FORMAT(5X,"TIME DIR ANG NRG FN RNG FN",4X,
5200 -"PERF INDEX"," STATE")
5210 0-
5220 C- COMPUTE ACM STATE
5230 C-
5300 100 DO 10 I=1.N
5400 STATE(I)=NUT
       IF (ATA (I) . LE. ATAOF. AND. AOT (I) . LE. AOTOF) STATE (I) = OFF
5500
5600 IF (ATA (I).LE.ATAWEP.AND.AUT (I).LE.AUTWEP.AND.R (I).GE.R1WEP.AND.
5700 -R(I).LE.R2WEP) STATE(I)=OFWEP
IF (ATA (I) .GE. (180.-AUTWEP) .AND.AUT (I) .GE. (180.-ATAWEP) .AND.
5900
6000 -R(I).GE.R1WEP.AND.R(I).LE.R2WEP) STATE(I) = DEFAT
6050 IF (R(I).GT.RNUT) STATE(I)=NUT
5050 C-
6070 C- COMPUTE NORMALIZED DIRECTIONAL ANGLE
6080 C-
6100 DA(I)=100.♦((180.-(AGT(I)+ATA(I)))/180.).
6200
      IF (DA(I)+0) 15,25,25
6210 C-
5220 C- BRANCH ON DIRECTIONAL ANGLE PLUS FOR OFFENSIVE FIGHTER
                                            MINUS FOR DEFENSIVE FIGHTER
6230 C-
5240 C-
6300
      15 CONTINUE
      RMAX=RMAX2
5400
5410
      ROPT=ROPTS
6420
      80=R02
      RG=RG2
5430
      EDEV=EDEVS
5440
5450
      F6=F62
     60 TO 45
5500
       25 RMAX=RMAX1
5500
      ROPT=ROPT1
5510
6520
      R0=R01
      R6=R61
6630
5540
      EDEV=EDEV1
6650 FG=FG1
      45 IF (RG.EQ. ROPT. OR. RG.EQ. RO. OR. FG. EQ. 0.) 60 TO 35
5700
```

```
6710 C-
5720 C- BEGIN COMPUTATION OF PERFORMANCE INDEX
6730 C-
5300 FSTR=F64((R6/RMAX) ◆ ((R6-R0PT) /RMAX ◆ (R6-R0) /RMAX) ◆◆2)
5900 GO TO 55
7000 35 FSTR=0.
7100 55 A=R(I)
      B= (A-ROPT) /RMAX
7200
7300
      C= (9-R0) /RMAX
7400 D=EXP(-8. +((A-RG)/ROPT)++2)
7500 E=FSTR+A/RMAX+(B+C+D)++2
7500
      FRN5(I) =E+1./(1.+500.+EXP(-12.+B))
7700 ESD=ES1(I)-ES2(I)
7800
      ESB=(ES1(I)+ES2(I))/2.
7900 DES=ESD/ESB
3000
      GEE=(2. +R(I)-RMAX-ROPT)/(RMAX-ROPT)
3100 EFF=EDEV+EXP(-4.+GEE++2)
3200' ECH=1./(1.+EDEV+EXP(-6.91+R(I)/R0))
9300
      K(I)=1.+(ECH+EFF-1.) ◆DES
3400
      IF (DA(I)+0)17,18,18
3500 17 K(I)=1./K(I)
8600 18 CONTINUE
8700 PI(I)=BA(I) +K(I) +(1.-FRNG(I))
3300
      IF (IPRINT.EQ. 1. OR. IPRINT. EQ. 5) 60 TO 986
3900
      60 TO 10
9000 986 CONTINUE
9200 IF (KOUNT.EQ.45) WRITE (IPRINT, 1003) (TITLE (KK), KK=1,50)
      IF (KOUNT.EQ. 45. AND. IPRINT.EQ. 5) WRITE (5, 301)
9300
      IF (KOUNT.EQ. 45. AND. IPRINT.EQ. 1) WRITE (1,30)
9310
9400 IF (KOUNT.EQ.45) KOUNT=0
9500 KOUNT=KOUNT+1
9550 IF (IPPINT.EQ.5) WRITE (5,278) I,R(I),ADT (I),ATA (I),ES1 (I),ES2 (I),
9560 -DA(I) +K(I) +FRNG(I) +PI(I) +STATE(I)
9570 278 FORMAT(6X,13,2X,15,2(2X,13),2(2X,15),2X,F6.2,2X,F7.4,
9580 -F7.4,2X,F10.2,5X,A1)
      IF (IPRINT.EQ.1) WRITE (1,20) I, DA(I), K(I), FRNG(I), PI(I), STATE (I)
9700
      20 FORMAT (5X.14.6X.F7.2.3X.F6.4.4X.F6.4.4X.F10.2.5X.A1)
      10 CONTINUE
9300
9900 KOUNT=1
10000 IF (IGRAF.EQ.1.QR.IGRAF.EQ.5) 60 TO 985
10100 GO TO 88
10200 935 CONTINUE
10210 C-
10220 C- BEGIN COMPUTATION FOR GRAPHICAL OUTPUT
10230 C-
10300 MT=1
10400 DO 44 I=1.H
10500 44 AA(I)=PI(I)
10600 WRITE (IGRAF, 2222)
10700 2222 FORMAT (1H1)
10800 WRITE(IGRAF, 1003) (TITLE(I), I=1,50)
10900
      WRITE (IGRAF, 1114)
11000 1114 FORMAT (25X." + PERFORMANCE INDEX",/
11100 -,1%, "T", 23%, "+ DIRECTIONAL ANGLE")
11200 WRITE(IGRAF.90)
11300 90 FORMAT(1X,"I",1X,"S",/1X,"M",1X,"E",3X,
11400 -"-100",2x,"-80",2x,"-60",3x,"-40",2x,"-20",
11500 -3x,"0",3x,"+20",2x,"+40",2x,"+60",2x,"+80",2x,"+100")
```

```
11500 DD 66 J=10.60
11700 BE (A = DD 7
11900 66 CONTINUE
11900 DD 666 J=10.60.5
12000 BE (J) =PLUS
13100
        566 CONTINUE
        WRITETIGRAF,77) (BE(J),J=10,60)
77 FORMAT(1x,"E",1x,"C",5x,51A1)
 18200
 15300
 12400
        DO 88 1=1.N
 12500 DO 99 J=10,60
 12600
        BE (J) =BLANK
                                           ( · · ·
 12700
        99 CONTINUE
 12800 BE (35) = DOT
 12900
        BE (60) =STATE (I)
 13000
        BE (10) =STATE (1)
        IF (DA(I).6T.99.9.OR.DA(I).LT.-99.9) 60 TO 4123
 13100
        IK=.25+DA(I)+35.5
 13200
 13300
        BE (IK) =PLUS
 13400
        60 TO 4133
 13500
        4123 BE (35) =XXX
        4133 CONTINUE
 13600
 13700
        IF (AA(I).6T.99.9.OR.AA(I).LT.-99.9)60 TO 9876
        J=.25+AA(I)+35.5
 13800
 13900
        BE (J) =STAR
 14000
        60 TO 7654
        9876 BE (35) =XXX
 14100
 14200
        7654 CONTINUE
 14400
        IF (KOUNT.EQ.45) WRITE (IGRAF, 1003) (TITLE (KK), KK=1,50)
        IF (KOUNT.EQ. 45) WRITE (IGRAF, 1114)
 14500
 14600
        IF (KOUNT.EQ.45) WRITE (IGRAF, 90)
 14700
        IF (KOUNT.EQ.45) KOUNT=0
 14300
        KOUNT=KOUNT+1
        WRITE (IGRAF, 11) MT, (BE(J), J=10,60)
 14900
 15000
        11 FORMAT (14,5X,51A1)
 15100
        MT=MT+1
 15200
        38 CONTINUE
 15210
        PRINT 411, IFIL
        411 FORMAT (5X, "ANOTHER FILE DONE ", 14)
 15220
 15230
        WRITE (4,786) N
 15240
        786 FORMAT (2X, 14)
        WRITE (4,785) (TITLE (JK), JK=1,50)
 15250
        785 FORMAT (2X, 50A1)
 15260
 15270
        DO 42 I=1.N
        IF (ABS (PI (I)).GT.99.9) PI (I)=0.
 15280
 15290
        42 CONTINUE
        WRITE (4,789) (PI(I), I=1,N)
 15300
 15400
        789 FORMAT(50(2X,9(F6.2,","),F6.2/))
 15410
        DO 1141 J=1+N
 15420
        IF (STATE (J) . EQ. OFWEP) ISTAT (J) =1
        IF (STATE (J).EQ. OFF) ISTAT (J) = 2
 15430
        IF (STATE (J).EQ.NUT) ISTAT (J) =3
IF (STATE (J).EQ.DEF) ISTAT (J) =4
 15440
 15450
 15460
        IF (STATE (J) . EQ. DEFAT) ISTAT (J) =5
 15470
        1141 CONTINUE
 15500
        WRITE(4,790) (ISTAT(I), I=1,N)
        790 FORMAT (50(2X,9(11,","),11/))
 15600
```

```
15625 IFIL=IFIL+1
15650 IF(IFIL.LE.NFILES) 60 TO 86
15700 PRINT 8111
15800 8111 FORMAT(////////5X, "REQUIRED FILE KEEPING TO SAVE DATA\\
\( \sigma \s
```

END QUIKLST 4.2 SEC.

PAIRED ANALYSIS PROGRAM OUTPUT
FOR EXAMPLE DATA SET

R PFINDX_ RUNNING

HOW MANY FILES AM I LOOKING AT

- 71_ WHERE DO YOU WANT DATA OUT, 1=HERE, 5=PRINTEROTHERS=MONE
- 71_ WHERE DO YOU WANT A GRAPH, 1=HERE, 5=PRINTEROTHERS=NONE
- 71_

```
A1M553Y A/C1 F4 TO A/C3 A4 ONE-ON-ONE
           A1M553Y A/C1 F4 TO A/C3 A4 ONE-ON-ONE
          INPUT CONSTANTS FOR THIS RUN
FIGHTER OFFENSIVE MAX RANGE
                                            24000.0 TARGET =
                                                                 30000.0
                                             6000.0 TARGET = .
           FIGHTER OPT MISSILE RANGE
                                                                  7500.0
                                              500.0 TARGET =
          FIGHTER MINIMUM RANGE (GUN)
                                                                   300.0
          FIGHTER GUN ENVELOPE RMAX
FIGHTER ENERGY RELEVENCE
                                             3000.0 TARGET =
                                                                  3500.0
                                             0.5000 TARGET =
                                                                  0.7500
           FIGHTER INTER-ENVELOPE PENAL
                                             0.0250 TARGET =
                                                                  0.0500
         OFFENSIVE ATA= 60.0 ADT=
OFF WEP ATA= 5.0ADT=
                                                90.0
         OFF WEP ATA= 5.0AOT=
OFF WEP RMAX= 9000.0RMIN=
                                            40.0
                                            3000.0
          FIGHT NUETRAL BEYOND 18000.0 RANGE
               DIR ANG HRG FN
                                    RNG FN PERF INDEX
    TIME
                                                              STATE
                                     0.0500
                 20.00
                          1.0360
                                                     19.68
       1
                                                                N
                 23.33
                          0.9333
                                     0.0277
                                                     21.17
                                                                11
                          0.9572
       3
                                     0.0168
                 26.11
                                                     24.57
                 28.89
                          0.9942
                                     0.0113
                                                     28.39
                          0.9946
                                                     31.22
                 31.67
                                     0.0036
                                                                0
                 34.44
                          0.9946
                                     0.0075
                                                     34.00
                          0.9938
                                     0.0075
                 36.11
                                                     35.62
                                                                0
                                     0.0064
                          0.9943
       8
                 38.89
                                                     38.42
       9
                          0.9889
                                     0.0101
                 40.56
                                                     39.70
                 40.56
                          0.9846
                                     0.0127
      10
                                                     39.43
                          0.9811
                                     0.0159
      11
                 41.67
                                                     40.23
                          0.9785
                                     0.0196
                 41.67
      12
                                                     39.97
      13
                 40.56
                          0.9792
                                     0.0237
                                                     38.77
                                                                0
                          0.9798
      14
                 41.67
                                     0.0272
                                                     39.71
                                                                0.9825
                                     0.0297
      15
                 41.67
                                                     39.72
                                                                0
                          0.9839
                                     0.0307
                                                     40.27
      16
                 42.22
                                                                0
                 43.33
                          0.9879
      17
                                     0.0298
                                                     41.54
                                                                0.9904
                                     0.0271
                                                     42.29
                 43.89
      18
                                                                0
                          0.9948
      19
                 43.89
                                     0.0231
                                                     42.65
                          0.9989
                                     0.0187
      30
                 45.00
                                                     44.11
                                                                0
      21
                 44.44
                          0.9999
                                     0.0143
                                                     43.80
                 42.78
                                     0.0105
      55
                          1.0016
                                                     42.39
                                                                0
      53
                 42.78
                        1.0018
                                     0.0075
                                                     42.53
                        1.0016
      24
                 37.78
                                     0.0053
                                                     37.64
      25
                 34.44
                         1.0012
                                   0.0037 .
                                                     34.36
                                     0.0027
      26
                 29.44
                         1.0008
                                                     29.39
      27
                 26.67
                        1.0006
                                     0.0020
                                                     26.63
                                     0.0018
                         1.0005
      28
                 24.44
                                                     24.41
      29
                 25.00
                          1.0004
                                    0.0023
                                                     24.95
                                                                0
                                     0.0027
      30
                         1.0004
                 22.78
                                                     22.73
                                                                0
                        1.0005
                 20.56
                                 . 0.0023
                                                     20.52
      31
                        1.0003
                 18.33
                                     0.0018
      35
                                                     18.31
      33
                          1.0012
                                     0.0019
                 21.11
                                                     21.10
                       1.0018
                                     0.0024
      34
                 20.00
                                                     19.99
                        1.0035
                                                     15.01
      35
                15.00
                                     0.0031
                        1.0053
                                     0.0040
      36
                 20.00
                                                     20.02
                                     0.0053
      37
                 15.56
                          1.0077
                                                     15.59
                 15.00
      38
                        1.0126
                                     0.0070
                                                     15.08
                                    0.0091
                         1.0177
      39
                 12.78
                                                     12.89
      40
                          1.0245
                                                     11.25
                 11.11
                                     0.0143
      41
                 9.44
                         1.0328
                                                      9.62
                                                                H
                  6.67
                          1.0400
                                     0.0171
                                                      6.82
      42
                                     0.0197
                          1.0472
      43
                  8.39
                                                      9.12
                                                                H
                  9.44
                          1.0503
                                     0.0220
                                                      9.70
```

1	A1M553Y A/C1	F4 TO A	/C3 A4 ONE-0	IN-OHE	
TIME	DIR ANG	HRG FH	RNG FN	PERF INDEX	STATE
45	7.22	1.0556	0.0237	7.44	
46	5.00	1.0578	0.0244	5.16	N
47	4.44	1.0602	0.0242	4.60	И
48	2.78	1.0587	0.0231	2.87	H
49	0.00	1.0573	0.0214	0.00	H
50	-1.67	0.9765	0.0065	-1.62	М
51	-7.22	0.9779	0.0060	-7.02	N
52	-12.22	0.9787	0.0054	-11.90	N
53	-13.89	0.9797	0.0049	-18.41	М
54	-24.44	0.9796	0.0046	-23.34	D
55 56	-23.89 -35.00	0.9792	0.0044	-28.16	D
57	-40.56	0.9779	0.0044	-34.08 -39.37	D D
58	-47.22	0.9712	0.0050	-45.63	D
59	-52.22	0.9656	0.0057	-50.14	D
60	-57.78	0.9590	0.0066	-55.05	D
61	-57.22	0.9499	0.0073	-53.93	D
62	-61.11	0.9384	0.0093	-56.81	D
63	-64.44	0.9236	0.0113	-58.85	D
64	-67.22	0.9073	0.0138	-60.15	D
65	-72.22	0.8877	0.0169	-63.03	D
66	-73.89	0.3549	0.0238	-61.66	D
67	-75.56	0.9365	0.0289	-61.38	D
68	-75.00	0.8173	0.0346	-59.17	D
69	-75.00	0.3045	0.0412	-57.85	D
70	-73.89	0.7892	0.0481	-55.51	D
71	-72.22	0.7788	0.0549	-53.16	D
72	-70.00	0.7697	0.0620	-50.53	D
73	-68.33	0.7574	0.0690	-48.18	D
74	-66.67	0.7510	0.0755	-46.29	D
75	-65.00	0.7432	0.0813	-44.38	D
76	-62.22	0.7411	0.0363	-42.13	D
77	-61.11	0.7499	0.0901	-41.70	D
78	-58.89	0.7583	0.0931	-40.49	D
79	-57.22	0.7677	0.0953	-39.74	D
80	-55.56	0.7745	0.0965	-38.87	D
81	-54.44	0.7752	0.0965	-38.13	D
92	-54.44	0.7733	0.0958	-38.07	D
83	-53.33	0.7725	0.0943	-37.31	D
84	-51.67	0.7747	0.0922	-36.34	D
85	-49.44	0.7761	0.0888	-34.96	D
96	-45.00	0.7839	0.0939	-32.32 -29.13	D
87	-40.00	0.7907	0.0790	-25.44	D
88 89	-34.44 -31.67	0.7979	0.0744	-23.71	n
• • • • • • • • • • • • • • • • • • • •					
•••	A1M553Y A/C1	HEG FN	C3 A4 UNE-U RNG FN	PERF INDEX	STATE
TIME	DIR ANG -28.33	0.8061	0.0672	-21.31	D
90 91	-23.33	0.8109	0.0652	-17.69	N
92	-18.33	0.3179	0.0633	-14.05	N
93	-15.56	0.3200	0.0626	-11.96	N
94	-10.56	0.3236	0.0625	-8.15	N
95	-7.78	0.8260	0.0632	-6.02	N
96	-4.44	0.8258	0.0649	-3.43	N
97	-1.67	0.8271	0.0578	-1.28	N
98	-0.56	0.8272	0.0716	-0.43	, N

i T IS	•	91M553	/ A/C1	• F	ERFOR	RMANC	I4 ONE E INDI IL ANGI	EX	HE		
ME	-100	-80	-50 -	-40	-50	0	+20	+40	+60	+30	+100
E.C	+	. +	+	+	,+	+	+	+	+	+	+
1	4					•	•				N
2 2	7						••				H
3 4	9						•				<u> </u>
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. 25	N							•			н
26	N										И
27	N										И
28	7 7					•					7
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31	Й						•				N
32	N						• 4				N
33	N						•				И
34	N					• *	•				7 7
35	N										N
37	H										N
33							•				N
39	74 N						•				N
40	N					•	•				N
41	N					. •					N
42	H										7.
33 34 35 36 37 39 40 41 42 43	N										N

1		A1M553Y 9/		AZC3 A DRMANC			NE		
Т				OTIONA					
1 3				211000	- 1110				
ME	-100	-30 -60	-40 -20	Ű	+20	+40	+60	+30	+100
45	. N								4
46	14			. •					4
47	*			. •					-4
43	14			. •					4
49	:4								4
50	**			•					1
51	N			• .					14
53	N			• .					- 14
53	H		•						H
54	D		•						D
55	D		• "						D
56	D			•					D
57	D			•					D
53	D			•					D
50	D			•					D To
61	D								D D
- 62	D			•					D
63	D	+•							D
64	D	+ •							ō
65	D	+ •							D
2.5	0	+ •							D
67	Ü	+ •							Ū
58	D								D
69	U	+ •							D
70	D	+ +							D
71	D	+ - •							D
72	D	**							D
73	D			•					D
74	D			•					D
75	D								0
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73 79 80	Ti								D
80	0	•							D
31	D	•							n
32	D	↓	•						D
31 32 33 34 35 36 37 59	0 0 0 0 0 0 0	•	•						D D D D
34	D	•							D
35	D								- Li
85	D		+ •						0 0
37	D		+ +						Ð
5.9	D D		+ •						D
39	D		* + •						Ð

```
A1M553Y A7C1 F4 TO A7C3 94 ONE-ON-ONE
1
                       . PERFORMANCE INDEX
 T
                        + DIRECTIONAL AMOLE
 IS
                                   +20 +40 +60 +30 +100
 7 E
      -100 -80 -60 -40 -20
  90
        D
                                                        D
  91
        H
                                                        14
  92
                                                        14
  93
        N
  94
  95
        M
  96
        H
  97
        H
  98
        11
ANOTHER FILE DONE 1
```

REQUIRED FILE KEEPING TO SAVE DATA ISH LOAD YOUR DATA FILE ADD REF SAVE REMOVE REF,ACM MAKE ACM AND REF SAVE

TH-TH-THATS ALL FOLKS

END PRINDX 14.9 SEC.

SECTION ANALYSIS PROGRAM

L SECTIOL

```
FILE: SECTI2 -08/16/76 10:01 AM.
100 BERRMES
200 FILE 1=TRMNL,UNIT=REMOTE
300 FILE REACM.UNITEDISK
400 FILE 3=BCM.UNIT=DISK
500 FILE 4=REF.UNIT=DISK
500 FILE 5=RANDY.UNIT=PRINTER BACKUP DISK
510 C-
515 C- REFERENCES ******* REFERENCES ******* REFERENCES
          1--- NATO RPT SA-03R-76 OF 26 JAN 1976
2--- NATO RPT TM-76-1SA OF 16 JUL 1976
3--- CENTER FOR NAVAL ANALYSES RPT CRC 274 OF NOV 1974
650 C-
630 0-
540 C-
650 C-
700 DIMENSION R1 (500) , R2 (500) , ES11 (500) , ES12 (500) , ES21 (500) ,
300 -ES22(500) -AGT1(500) -AGT2(500) -ATA1(500) -ATA2(500) -
900 -TITLE1 (50) .TITLE2 (50) .PI1 (500) .PI2 (500) .ISTAT1 (500) .
1000 -ISTATE (500) , PIS (500) , PHI (500) , STATE (500)
1100 DIMENSION AA (500) , BE (500)
1200 DIMENSION CONCO (500)
1300 DIMENSION ISTAT (500)
1400 DATA BLANK, DOT, STAR, XXX, PLUS/" ", ". ", ", ", "X", "+"/
1500 DATA DOLL/"$"/
1600 DATA OFWEP, OFF, DEF, NUT, DEFAT, TRADE/"W", "O", "D", "N", "F", "T"/
1601 C-
1602 C- MANEUVER CONVERSION DATA WEOFFENSIVE WEAPONS
1603 C-
                                      O=OFFENSIVE
                                      N=NEUTRAL
1604 C-
                                      D=DEFENSIVE
1605 C-
                                      F=FATAL DEFENSIVE
1606 C-
                                       T=TRADEOFF
1607 C-
1603 C-
1610 PRINT 433
1620 433 FORMAT (5%, "HOW MANY FILES AM I LOOKING AT ")
      READ(1./) NEILES
1630
1640
      IFIL=1
1700 PRINT 434
1800 434 FORMAT(5%, "WHERE DO YOU WANT DATA OUT. 1=HERE, 5=PRINTER",
1900 -"OTHERS=NONE")
2000 READ(1./) IPRINT
2100 PRINT 435
2200 435 FORMAT (5%, "WHERE DO YOU WANT A GRAPH, 1=HERE, 5=PRINTER",
2300 -"OTHERS=NONE")
2400 READ(1,/) IGRAF
      WRITE (1,775)
2450
8455 86 CONTINUE
2460 775 FORMAT(2X,"GO TO SLEEP, I WILL CALL WHEN I AM READY")
2465 C-
2470 C- BEGIN INPUT FROM PERFORMANCE INDEX PROGRAM
2480 C- PAIR 1 DATA IS LOCATED IN DISK FILE ACM
2485 C- PAIR 2 DATA IS LOCATED IN DISK FILE BOM
8490 C-
2500 PEAD(2,7) N1
2700 READ(2.123) (TITLE1(I).I=1.50)
2800 123 FORMAT (50A1)
```

```
READ(2,/) (PI1(I), I=1,N1)
2900
      READ(2,/) (ISTAT1(D, I=1,N1)
3000
      READ (3, /) N2
3100
      READ(3,123) (TITLE2(1),1=1,50)
3300
      READ(3,/) (PI2(I), I=1,N2)
3400
3500
      READ(3, /) (ISTAT2(I), I=1, N2)
3600
     H=H1
3700
     IF (N2.LT.N1) N=N2
3800
      PHIT=0.
3810 0-
3820 C- BEGIN COMPUTATION OF SECTION PERFORMANCE INDEX BY .
3830 C- MAGNITUDE SUM METHOD OF REFERENCE 2
3340 C-
3900 DO 10 I=1.N
4000 PI1SQ=PI1(I) +ABS(PI1(I))
4100
      ((1)SIQ) SAR+(1)SIQ=02SIQ
      RAD=ABS(PI1SQ+PI2SQ)
4200
4300 IF (ABS (RAD) .LT. 0.1) PIS(I) =0.
4400 IF (ABS (RAD) .LT. 0.1) 60 TO 3
4500
      SIGN=(PI1SQ+PI2SQ)/RAD
      PIS(I)=SIGN+SQRT(RAD/2.)
4600
4601
     3 CONTINUE
4602 C-
4603 C- BEGIN COMPUTATION OF CONVERSION COEFFICIENT AS OUTLINED
4604 C- IN THE TEXT
4605 C-
4700 IF (ABS(PI1(I)).6T.100.) CONCO(I)=0.
      IF (ABS(PI2(I)).6T.100.) CONCO(I)=0.
4800
4900
     IF (ABS(PI1(I)).6T.100..OR.ABS(PI2(I)).6T.100.) 60 TO 9
5000 IF ((PI1(I).6T.30..AND.PI2(I),LT.30.).OR. (PI2(I).6T.30..AND.
5100 -PI1(I).LT.30.>> 60 TO 5
5200 \quad CONCO(I) = PIS(I)
5300 GO TO 9
5400 5 IF (ABS(PI1(I)).LT.75..AND.ABS(PI2(I)).LT.75.) 60 TO 6
     IF (ABS(PI1(I)).LT.0.1) PI1(I)=0.1
5401
      IF (ABS (PI2(I)).LT.0.1) PI2(I)=0.1
5402
5500 IF (ABS(PI1(I)).6T.ABS(PI2(I))) CONCO(I) =SORT(PI1(I) ++2+
5600 -(1.-ABS(PI2(I)/400.))) +PI1(I)/ABS(PI1(I))
     IF (ABS(PI2(I)).GT.ABS(PI1(I))) CONCO(I) = SQRT(PI2(I)++2+
5800 -(1.-ABS(PI1(I)/400.))) +PI2(I)/ABS(PI2(I))
5900 IF(ABS(PI1(I)).6T.75..AND.ABS(PI2(I)).6T.75.) CONCO(I)=PIS(I)
6000 60 TO 9
6100 6 IF (PI1(I).6T.PI2(I))
5200 -CONCO(I)=SORT(PI1(I)++2+(1.-ABS(PI2(I))/75.))
5300 IF (PI2(I).5T.PI1(I))
6400 -COMCO(I) = SORT (PI2(I) ••2•(1.-ABS(PI1(I))/75.))
     9 XK1=ABS(PI1(I)-PIS(I))
6500
5600 XK2=ABS(PI2(I)-PIS(I))
5700 DEN=XK2
5800 XNUM=XK1

5900 IF (XK1.GT.XK2) DEN=XK1

7000 IF (XK1.GT.XK2) XNUM=XK2

7050 IF (DEN.LT.0.1) PHI(I)=0.
7100
      PHI (I) =XNUM/DEN
7200 10 PHIT=PHIT+PHI(I)
7300 PHIT=PHIT/N
```

```
7310 C-
7320 C- COMPUTE ACM STATE FOR TWO ON ONE PER REFERENCE 3
7330 C-
7400 DO 20 I=1.N
7500
     STATE (I) = DEF
7600 IF (ISTAT1 (D.EQ.1. AND. ISTAT2 (D.NE.5) STATE (D = OFWEP
      IF (ISTATE (I) .EQ. 1. AND. ISTAT1 (I) .NE. 5) STATE (I) = OFWEP
7700
7800 IF (ISTAT1 (I) .EQ. 1. AND. ISTAT2 (I) .EQ. 5) STATE (I) =TRADE
7900 IF(ISTAT2(I).EQ.1.AND.ISTAT1(I).EQ.5) STATE(I)=TRADE
      IF (ISTATE (I).EQ.2.OR.ISTAT1 (I).EQ.2) STATE (I) =OFF
3000
      IF (ISTAT) (D.EQ. 3. AND. ISTAT2 (D.EQ. 3) STATE (D = NUT
3100
8200 IF (ISTATI (I).EQ.5.AND. ISTAT2(I).NE.1) STATE (I) = DEFAT
3300 IF (1STAT2(I).EQ.5.AND.ISTAT1(I).NE.1) STATE(I) = DEFAT
8400 20 CONTINUE
3500
      SUM=0.
9500 DO 30 J=1.N
30 SUM=SUM+PHI(J) ◆◆2
5800 COURD=1.-SQRT(SUM/N)
3310 C-
3820 C- BEGIN PRINT OF OUTPUT
8830 C-
8900 IF (IPRINT.NE.1.AND.IPRINT.NE.5) 60 TO 40
9000 WRITE (IPRINT, 1003) (TITLE1(I), I=1,50), (TITLE2(I), I=1,50)
9100 1003 FORMAT (1H1, 10X, 50A1/11X, 50A1)
9200 WRITE (IPRINT, 301)
9300 301 FORMAT (5X, "TIME
                              PERF
                                       PERF
                                                 PERF
                                                         CONVERSION >>
          N STATE"/
                 5×,"
9400 -
                            INDEX
                                    INDEX
                                                INDEX
                                                         COEFFICHT W
          N (SECTION) "/
9500 -
                 5X,"
                           PAIR1
                                      PAIR2
                                                SECTH")
9600 KOUNT=1
9610 C-
9520 C- BEGIN GRAPHICAL COMPUTATIONS FOR OUTPUT GRAPH
9630 C-
9700
      DO 40 J=1,N
9800 IF (KOUNT.EQ.45.) WRITE (IPRINT, 1003) (TITLE1(I), I=1,50),
9900 - (TITLE2(I), I=1,50)
10000 IF (KOUNT.EQ.45) WRITE (IPRINT: 301)
10100 IF (KOUNT.EQ.45) KOUNT=0
10200 KOUNT=KOUNT+1
10300 WRITE(IPRINT.278) J.PI1(J),PI2(J),PIS(J).CONCO(J).STATE(J)
       278 FORMAT (5X, 13, 4 (3X, F6.2), 9X, A1)
10400
       40 CONTINUE
10500
      IF (IPRINT.EQ.1.OR.IPRINT.EQ.5) WRITE (IPRINT,909) PHIT, COORD
10600
       909 FORMAT(10X, "SECT COORD = ",F6.4,5X, "CONSISTENCY = ",F6.4)
10700
10300
       MT=1
      DO 44 I=1.N
10900
11000 44 AA(I)=PIS(I)
11100 IF (IGRAF.NE.1.AND.1GRAF.NE.5) GO TO 50
       KOUNT=1
11200
11300 WRITE(IGRAF.1003) (TITLE1(KK).KK=1.50).(TITLE2(KK).KK=1.50)
11400 WRITE (IGRAF, 1114)
11500 1114 FORMAT(25x," * SECTION INDEX + FOR TRADE-OFF" . / 25x,
11600 -"# CONVERSION COEFFICIENT "./.1X,"T"J
11700 WRITE (IGRAF, 90)
11800 90 FORMAT(1X+"I"+1X+"S"+/1X+"M"+1X+"E"+3X+
11900 -"-100",2%,"-80",2%,"-60",2%,"-40",2%,"-20",
```

```
12000 -3%, "0", 3%, "+20", 2%, "+40", 2%, "+60", 2%, "+80", 2%, "+100")
12100 DU 66 J=10.60
13200 BE(J)=DOT
12300 66 CONTINUE
13400 DO 566 J=10.60.5
18500 BE (J) =PLUS
12600. 666 CGHTINUE
12700 WRITE(IGRAF.77) (BE(J).J=10.60)
18800 77 FORMAT(1X."E".1X."C".5X.5141)
12900 DO 88 I=1.N
13000 DO 99 J=10.60
13100 BE ( ) = BLANK
13200 99 CONTINUE
13300 BE (35) = DOT
13400 BE(60) =STATE(I)
13500 BE(10)=STATE(I)
13600 IF(CONCO(I).6T.99.9.GR.CONCO(I).LT.-99.9) 60 TO 4123
13700 K=.25+CONCO(I)+35.5
13800 BE(K)=DOLL
13900 60 TO 4133
14000 4123 BE(35) =XXX
14100 4133 CONTINUE
14200 IF (AA(I).51.99.9.0R.AA(I).LT.-99.9)60 TO 9876
14300
       J=.25 AA (1)+35.5
14400 BE (J) = STAR
14500 IF ((PI1(I).GT.75..AND.PI2(I).LT.-75.).GR.(PI1(I).LT.-75..
14600 -AND.P12(I).5T.75.)) BE(J)=PLUS
14700 60 TO 7654
14800 9876 BE(35)=XXX
14900 7654 CONTINUE
15000 IF(KOUNT.E0.45) WRITE(IGRAF,1003) (TITLE1(KK),KK=1,50),
15100 - (TITLE2 (KK) , KK=1,50)
15200 IF (KOUNT.EQ.45) WRITE (IGRAF, 1114)
15300 IF (KOUNT.EQ.45) WRITE (IGRAF.90)
15400 IF (KOUNT.EQ.45) KOUNT=0
15500 KOUNT=KOUNT+1
15600 WRITE(IGRAF, 11) MT, (BE(J), J=10,60)
15700 11 FORMAT (14,5X,51A1)
15800 MT=MT+1
15900 33 CONTINUE
16000 50 CONTINUE
16010 WRITE(1,776)
16020
       776 FORMAT (2X, "WAKE UP, I HAVE DONE ANOTHER FILE")
16030 WRITE(1,123) (TITLE1(I),I≈1,50)
16031 C-
15032 C- CREATE AN OUTPUT FILE ON DISK (REF) FOR FURTHER ANALYSIS
16033 C-
16050 WRITE (4.777) N
16060 777 FORMAT (2X, 14)
       WRITE(4,789) (PIS(I), I=1,N)
15100
       WRITE (4,787) (TITLE1(I), I=1,50), (TITLE2(I), I=1,50)
15125
16150 787 FORMAT(2X,5041,7,2X,5041)
16200 789 FORMAT(50(2X,9(F6.2,","),F6.2/)
15300 DO 1141 J=1.N
15400 IF(STATE(J).EQ.OFWEP) ISTAT(J)=1
16500 IF (STATE (J) .EQ. OFF) ISTAT (J) =2
```

```
16800 IF(STATE(J).E0.NUT) ISTAT(J)=3
18700 IF(STATE(J).EQ.DEF) ISTAT(J)=4
16806 IF (STATE (J).50.DEFAT) ISTAT (J)=5
19900 IF(STATE(J).50.TRADE) ISTAT(J)=6
17000 1141 CONTINUE
17100 WRITE(4,790) (ISTAT(I),I≈1,N)
17200
      790 FORMAT(50(2X,9(I1,","),I1/))
17300 WRITE(4,789) (CONCO(I),I=1,N)
17350
      IFIL=IFIL+1
      IF (IFIL.LE.NFILES) 60 TO 86
17360
17400
      8765 CALL EXIT
17500
      END
```

END QUIKLST 3.1 SEC.

SECTION ANALYSIS PROGRAM OUTPUT
FOR EXAMPLE DATA SET

R SECTIEL RUNNING

HOW MANY FILES AM I LOOKING AT

71_ WHERE DO YOU WANT DATA OUT, 1=HERE, 5=PRINTEROTHERS=NONE

71_ WHERE BO YOU WANT A GRAPH, 1-UCOC, 5-00INTERSTUCES-MONE

WHERE DO YOU WANT A GRAPH, 1=HERE, 5=PRINTEROTHERS=NONE
71_
50 TO SLEEP, I WILL CALL WHEN I AM READY

TM 77-2 SA

1

	ac#56	4Y 1 TO	3 8 ON 1	TEST 5/40,3-9	9K,60/90,18KM
	BCMU641				60/90,13KMAX
TIME	PERE	PERF	PERF	CONVERSION	
	INDEX	INDEX	INDEX		
	PAIRI	PAIRS	SECTH	202 (120 ()	130011011
1	-10.43	-2.53	-7.59	-7.59	М
e .	-14.57	-3.56		-10.51	N
3	-17.59	-4.27	-12.30	-12.30	N
4				-14.59	
	-19.94	-5.30	-14.59		ц
5	-21.53	-6.20	-15.88	-15.88	N
6	-22.55	-7.43	-15.80	-16.30	М
7	-33.44	-7.61	-15.75	-16.76	И
3	-22.50	-8.43	-17.06	-17.06	Н
9	-22.16	-3.71	-15.34	-16.84	И
10	-22.14	-8.81	-16.35	-16.85	N
11	-21.63	-9.34	-16.43	-16.43	N.
1 ≥	-30.31	-9.51	-16.13	-16.13	N
13	-19.16	-8.21	-14.74	-14.74	И
14	-17.52	-6.07	-13.11	-13.11	И
15	-16.68	-4.71	-12.21	-12.21	4
16	-14.44	-3.49	-10.50	-10.50	N
17	-13.40	-2.09	-9.59	-9.59	И
18	-11.35	-0.54	-3.39	-8.39	N
19	-10.50	1.12	-7.38	-7.38	N
20	-9.32	3.34	-6.15	-6.15	N
21	-7.52	6.68	-2.52	-2.52	N
55	-6.89	8.11	3.02	3.02	N
53	-5.77	19.10	12.13	12.13	N
24	-4.20	22.07	15.32	15.32	N
25	-1.71	23.42	20.05	20.06	N
26	0.00	30.27	21.40		N
27	1.96	31.33	22.20	30.93	и
29	3.34	25.11	13.61	18.61	N
29	4.46	19.49	14.14	. 14.14	N
39	5.77	15.03	11.42	11.42	N
31	5.94	15.70	11.37	11.37	Ä
32	5.45	15.70	12.77	12.77	
33	7.77	12.41	10.35	10.35	N
34	9.31	3.43	8.90	3.90	N
35	10.67	5.09	3.36 8.53	9.36 9.53	N
36	12.06	0.00	9.23		
37	13.10	-5.01		3.23	H
38	14.35	-14.26	1.13	1.13	
39	15.85	-19.25	-7.72	-7.73	Ŋ
40	19.71	-22.05	-3.25	-9.25	Н
41	21.31	-37.62	-13.42	-12.42	Ņ.
43	24.39	-34.30	-17.06	-17.06	D
43	28.84	-38.78	-19.37	-19.27	D
44	32.72	-45.23	-88.13	20.50	D

1		9CM56	4Y 1 TO 3	BON I T	EST 5/40.3-	9K,50/90,18KM
		BCM564	2 04 1. 2	TO 3 TES	T 5/40,3-9k	:,60/90,18KMAX
	TIME	PERF	PERF	PERF	CONVERSIO	M STATE .
		INDEX	KEUNI	INDEX	COEFFICHT	(SECTION)
		PAIR1	PAIRS	SECTH		
	45		-51.77	-25.64	20.56	D
	46	41.69			20.02	D
	47	46.27			17.93	D
	43	50.15	-69.74	-34.27	13.23	D
	49	53.19	-74.23	-36.61	5.39	0
	50	56.48	-79.85	-39.96	-74.00	F
	51	61.57	-82.20	-33.51	-75.51	F
	53	55.15	-32.33	-36.22		F
	53	70.45		-33.15		F
	54	74.67				F .
	55	73.10				J
	56					0
	57		-96.21			0
	58	85.73	-30.62		20.62	a
	59	36.90	-76.11	29.66	29.66	0
	60	34.26	-71.60	31.41	76.35	0
	61	92.32	-65.41	35.34	75,29	٥
	56	30.86	-59.66	39.35	74.70	<u> </u>
	63	78.21	-51.32			0
	64	75.86				<u>a</u>
	65	72.02				ā
	66		-19.76		59.39	0
	67	63.60	-10.03	43.69	58.27	ם י
	68	59.06	2.35	41.79	59.13	<u> </u>
	69	51.70	9.44	37.16 35.39	43.34	ם
	70	44.79	22.33 29.36		37.53	3
		37.79				0
	72 73	32.66 26.70	34.41 35.50			N N
	74	23.63	34.51		23.64	N
	75	23.84	28.99	26.54	26.54	N
	76	22.31	26.13		24.55	N
	77	21.74	22.81	22.23	22.28	N
	73	20.69	21.82	21.26	21.26	N
	79	20.23	24.07	22.23	22.23	N
	80	20.61	82.91	21.79		r i
	31	20.93	21.58	21.23	21.28	14
	88	21.59	20.57	21.09		н
	93	22.69	13.70	20.79	20.79	a
	34	22.61	16.37	19.95	19.95	й
	35	24.16	15.03	20.14	20.14	N
	35	25.72	18.95	20.36	20.36	N N
	37	26.18	11.03		20.10	4
	93	27.79	9.74	20.38	20.33	н
	39	31.40	3.29	22.96	29.51	N

1		ACM564 BCM564 8				-9K,60/90,18KM K,60/90,18KMAX
	TIME	PERF	PERF	PERF		
	TIME				CONVERSI	
		INDEX		INDEX	CUEFFICH	T (SECTION)
		PAIR1	PAIRS	SECTH	37.50	
	90	39.46	7.20	23.36	37.52	4
	91	43.77	7.12	31.36	41.54	a
	92	60.34	6.89	42.94	57.50	3
	93	67.66	7.10	48.11	64.38	٥
	94	38.78	5.82	27.84	36.97	И
	95	16.03	6.31	12.13	12.18	H
	96	7.73	6.23	7.02	7.02	N
	97	-0.55	5.70	4.01	4.01	И
	93	-9.40	5.44	-5.42	-5.42	N
	99	-21.05	5.09	-14.44	-14.44	N
	100	-37.72	5.34	-26.40	-26.40	D
	101	-53.27	5.56	-37.46	-37.46	D
	102	-62.11	5.41	-43.75	-43.75	D
	103	-64.73	5.48	-45.61	-45.61	D
	104	-59.93	5.12	-42.88	-42.22	D
	105	-55.49	5.13	-39.07	-39.07	И
	105	-50.77	5.01	-35.72	-35.72	И
	107	-43.95	4.54	-34.46	-34.46	N
	103	-43.49	4.01	-34.17	-34.17	И
	109	-45.40	3.40	-32.01	-32.01	N
	110	-40.93	3.03	-23.86	-28.86	N
	111	-38.62	2.63	-27.24	-27.24	N
	112	-36.84	2.42	-25.99	-25.99	N
	113	-35.56	2.31	-25.09	-25.09	н
	114	-33.13	2.20	-23.37	-23.37	H
	115	-33.36	2.28	-23.53	-23.53	N
	116	-34.02	2.32	-24.00	-24.00	N
	117	-34.56	2.34	-24.38	-24.38	N
	118	-34.32	2.63	-24.20	-24.20	N
	119	-29.77	2.97		-20.95	N
	120	-27.63	3.60	-19.37	-19.37	И
	121	-25.92	4.71	-18.02	-18.02	Н
	122	-24.16	6.61	-15.43	-16.43	H
	123	-22.40	3.72	-14.59	-14.59	N
	124	-23.40	10.53	-14.74	-14.74	N
	125	-23.42	13.14	-13.71	-13.71	N
	126	-22.19	15.52	-11.21	-11.21	И
	127	-20.39	15.03	-9.74	-9.74	N
	123	-18.76	12.49	-9.90	-9.90	'n
	129	-13.42	10.13		-10.33	7
	130	-15.75	5.07	-10.88 -11.30	-11.30	N
	131		2.47			4
		-14.47 -11.52		-10.09	-10.09	
	132	-8.93	0.50	-9.13	-3.13	7 1
	133		4.05	-5.52 .	-5.62	N
	134	-7.35	5.69	-3.83	-3.33	6 4

1					ST 5/40.3-9K.	60/90,13KM
		BCM564 2	DN 1, 2	TO 3 TEST	5/40,3-9K,60	790,18KMAX
	TIME	PERF	PERF	PERF	CONVERSION	STATE
		INDEX	INDEX	INDEX		SECTION
		PAIR1	PAIR2	SECTH		
	135	-7.18	11.22	6.10	6.10	N
	136	-5.00	16.13	10.83	10.38	М
	137	-0.78	84.48	17.30	17.30	И
	138	1.35	29.93	21.22	21.22	0
	139	6.85	29.37	21.23	21.23	0
	140	11.75	33.83	25.32	31.07	N
	141	18.22	41.11	31.80	35.77	N
	142	20.73	43.39	34.00	36.91	N
	143	22.70	47.35	37.13	39.54	יי פ
	144	23.39	49.65	38.81	41.19	9
	145	23.20	51.98	40.25	43.20	3 (
	146	22.75	55.43	42.37	46.27	J .
	147	22.61	59.96		50.11	0
	143	21.70	63.36	47.36	53.41	3
	149	23.63	66 77	50.03	55.26	0
	150	27.20	71.79	54.28	57.31	ā
	151	30.76	76.76	58.47	58.47	ā
	152	34.94	77.83	60.33	60.33	٥
	153	33.61	79.34	61.76	61.76	
	154	41.24	79.37	63.25	63.25	a
	155	46.17	77.04		63.51	0
	156	51.64	71.92	62.61	62.61	0
	157	55.15	69.06	62.49	62.49	
	155	58.44	65.11	61.86	61.36	0
	159	57.99	62.23	60.17	60.17	ā
	160	55.67	60.03	57.89	57.89	j
	151	53.54	57.10	55.35	55.35	i
	163	52.47	53.09	52.79	52.79	0
	163	50.26	48.95	49.61	49.61	3
	164	46.60	48.61		47.62	0
		SECT COORD	= 0.5645	CONSI	[STENCY = 0.4]	010
	100					

1			564Y 1 4 2 GN	TO 1,	3 2 0N 2 TO 3 SECTIO CONVER	H IN	DEX	0,3-9 + FOR	K.60/	90,18	KMAX
Ţ				•							
IS ME	-100	-80	-60	-40	-20	0	+20	+40	+60	+30	+100
EC	+	+	+	. +	+	. +	+	+	+	+	+
	N				•						N
1 2 3	14										ri
3	14				•						H
4	14				•						H
5	N				•	-					11
6 7	N				•						H
7	Н				•						И
8	N				•						н
9	Н					•					И
10	Н										11
11	N					•					14
13	н					•					H
14	N										И
15	N										N
16	H										N
17	N				•						N ·
18	- 11				•						N
19	N				•						N
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53	И					•	•				Н
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25	н					•		•			11
27	N					•		\$ \$			N
23	N										N
29	N						•				И
30	N						•				N
31	N						•				N
	4						•				N
32 33 34 35 36 37	N						•				N
34	М					. •					N
35	N					. •					H H
36	H H					• •					Й
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38	N										H
37	N										7
39 40 41 42 43 44	11										7 7 D D
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44	D				•		*	•			D
A FUNDAMENTAL STREET								14			

2 1											
4 E	-100 D	-30	-60	-40	• -20		*20	+40	+60	+30	+10 D
46 47 48	D D					•	*				D
49	0 5	8		·		. 5					0 0 5
51 52	F	3		•							F
53	F	3		Ĭ.	4						FIFE
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56 57	0				•	•					0
58 59	0						•			\	0
60 61	0							•		5	0
62 63	0							:		8	0
64 65	0							*.	\$	3	0
66 67	0								8		0
68 69	٥								8		000
70	0			216				•			0
71	D N						•				7.0
73 74	7 7						•				7 7
75 76	H										4
77 78	4						•				7
79 30	71						•				7
31	N N						:				14
33	0						•				۵
34 35	N N							•			7
35 37	H					:					7
33	N						• **				7 7

1 		ACMS BCMS64	564Y 1 1 2 ON	10	SECTI	3 TES	EST 5 T 5/4 DEX COEF	0•3-9 • FOR	K,60/ TRAD	90,13	KMAX
1 2			MBOH!		1122						
ME	-100	-30	-60	-40	-20	0	+20	+40	+60	+30	+100
90	7					•	•	£ .			И
91	0					•		• 1			0
98								45.00	1		0
93 94									3		7
95	H							D			N
96	N										N
97	N					•					N
98	И										N
99	N										N
100	D										D
101	D										D
102	D			•							D
103	D			•							D
104	D			•							D
105	N P			•							H
105	N	*									N
107	N										И
103	N										14
109	N			4	•						N
110	H				•						N
111	H				•						N
112	N				•	•					И
113	H				•	•					М
. 114	N				•						N .
115	Н				•	•					И
116	И				•	•					И
117	Ч					•					И
113	H					•					H
119	7										N
120	H					•					И
121											N
122	H				-						14
124	N										И
125	И										И
126	N										И
127	N					•		4.50			N
123	N					• .		4 (4)			N
129	N				•						4
130	N										N
131	N										N
132	. 14					• .					N
133	11					٠.					N
134	N					٠.					N

```
ACM564Y 1 TO 3 2 ON 1 TEST 5/40,3-9K,60/90,13KM
1
           BCM564 2 ON 1, 2 TO 3 TEST 5/40,3-9K,60/90,13KMAX
                      . SECTION INDEX + FOR TRADE-OFF
                       & CONVERSION COEFFICIENT
 T
 1 3
                               0 +20 +40 +60 +30 +100
 ME
      -100 -80 -60 -40 -20
      :4
 135
                                                      14
 136
       N
 137
       14
                                                      14
 133
        0
                                                      J
 139
        140
 141
        M
 142
 143
        J
                                                      0
        O
 144
                                                      0
        0
 145
                                                      146
        0
        0
 147
                                                  0
        0
143
        0
 149
        9
 150
        0
151
                                                  0
        152
                                                     0
 153
                                                     0
154
                                                     O
 155
        0
       0
156
      00
 157
 158
                                                     O
        0
 159
                                                      0
 160
        0
                                                      3
        161
                                                      O
                                                     J
 162
        0
 163
        0
                                                     0
 164
        0
 WAKE UP, I HAVE DONE ANOTHER FILE
 ACM564Y 1 TO 3 2 ON 1 TEST 5/40,3-9K,60/90,18KM
```

END SECT12 17.4 SEC.

STOCHASTIC ANALYSIS PROGRAM

```
FILE: STACM6 -08/23/76 10:33 AM.
100 BERRMES
200 FILE 1=TRMNL, UNIT=REMOTE
300 FILE 2=ACM, UNIT=DISK
400 FILE 3=BCM.UNIT=DISK
500 FILE
          4=REF,UNIT=DISK
         5=RANDY.UNIT=PRINTER BACKUP DISK
600 FILE
700 FILE 6=CCM, UNIT=DISK
300 FILE 7=OPT, UNIT=DISK
900
    INTEGER GRAFOP
1000 DATA PLUS/"+"/
1100 DATA BLANK/" "/
1200 DATA DOT/"."/
      DATA STAR/"+"/
1300
1400 DATA DOLL/"$"/
1500 DATA AT/"#"/
1600 DIMENSION TPCALE (5,51)
     DIMENSION N(40), PIS(40,300), SECTIT(40,140), ISTATS(40,300),
1700
1800 -CONCO (40,300), NPAIR (30), PARTIT (80,70), PIPAIR (80,300),
1900 -ISTATP(80,300),A(300),B(300),KPIS(300),FPIS(250,120),
2000 -FREQ(300), CUMPIS(250,120), CUMP(300), PISMN(300), PISDEV(300),
2100 -PISM3(300),PISM4(300),ANS(4),FCC(250,120),CUMPCC(250,120)
2200 DIMENSION CCMN(300), CCDEV(300), CCM3(300), CCM4(300), KIPAIR(300),
2300 -FPIP(250,120),CUMPIP(250,120),PIPMN(300),PIPBEV(300),PIPM3(300),
2400 -PIPM4(300), NCS(6,6), CPS(6,6), TC(6), MXX(300), NAME1(40), NAME2(40)
2500 DIMENSION IFL(6),ITIS(6,300),TSCALE(6,51),TFREQ(6,51),TCUMP(6,51),
2600 -TMEAN(6), TDEV(6), TMOM3(6), TMOM4(6), CPP(5,5), NCP(5,5), ITIP(5,300),
2700 -TPFREQ(5,51),TPCUMP(5,51),TPMEAN(5),TPDEV(5),TPMOM3(5),TPMOM4(5)
2800 DIMENSION NAMES (40) , NAME4 (40)
      DIMENSION NAMES (40)
2300
     DIMENSION IFM (6)
2910
3000 C- READ IN REQUIRED CONSTANTS FOR DATA MANAGEMENT
3100 C-
     READ (7, /) NFILES, IPRINT, IGRAF, ICALC, DELTA, ICOMP
3200
      GRAFOP=IGRAF/ABS(IGRAF)
3300
3400
     IGRAF=ABS (IGRAF)
3500
     NCK=IGRAF/ICOMP
3600
      NKC=IGRAF/ICOMP+0.999
     IF (NCK. NE. NKC) IGRAF=ICOMP
3700
3800
     101 FORMAT (40A1)
3900
     READ (7,101) (NAME1 (1), I=1,40)
4000
      READ (7,101) (NAME2 (1) , I=1,40)
      READ (7,101) (NAME3(I), I=1,40)
4100
      READ (7,101) (NAME4(I), I=1,40)
4200
     READ (7,101) (NAMES (1), I=1,40)
4300
4400 C-
4500 C-
4600 C- NFILES IS THE NUMBER OF DATA FILES TO BE REDUCED
4700 C-
4300 C-
4900 C- IPRINT IS OUTPUT OPTION, 1 FOR TERMINAL 5 FOR PRINTER
5000 C-
5100 C-
5200 C- IGRAF IS PLOTTING TIME INTERVAL + FOR FROUENCY DATA - FOR FEQ &
5300,6-
        CUMULATIVE PROBABILITY
5400 C-
```

```
5500 C-
5600 C- ICALC IS CALCULATION OPTION 1 FOR CONVERSION COEFF & SECTION PI
5700 C-
                                        2 FOR PAIRED PI IN ADDITION
                                        3 FOR MANEUVER CONVERSION OF SECTION
                                            IN ADDITION TO 182
5900 0-
6000 C-
                                         4 FOR ALL ABOVE PLUS IND
                                            PAIRED MAN CONV
5100 C-
                       5 FOR SECTION DATA ONLY (ALL COMPUTATIONS)
6200 C-
6210 C- DELTA IS GRID SIZE FOR CONTINUOUS COMPUTATIONS IN RANGE OF ...
           N +/-100
6815 0-
6300 C- ICOMP IS THE FREQUENCY OF DATA COMPUTATION IN INTEGER SECONDS
6400 C- NAME1 IS THE TITLE FOR FREQUENCY DATA GRAPH
6500 C- NAME2 IS THE TITLE FOR PERFORMANCE INDEX GRAPH
6600 C-NAMES IS THE TITLE FOR CUMULATIVE PROBABILITY GRAPH
5700 C-NAME4 IS THE TITLE FOR CONVERSION COEFFICIENT GRAPHS
6800 C- NAMES IS THE TITLE FOR TIME IN STATE GRAPHS
6900 C- N IS NUMBER OF PTS IN SECTION FILES--IT HAS NEILES VALUES
7000 C- NPAIR IS THE NUMBER OF POINTS IN PAIRED FILES IT HAS
7100 C-
                               2. ONFILES VALUES
7200 C- FOR A 2 V 1 ENGAGEMENT
7300 C- PIS ARE THE SECTION PERFORMANCE INDICES IT HAS N(I) VALUES
7400 C-
                               PER DATA FILE
7500 C- ISTATS ARE THE MANEUVER CONVERSION STATES--N(I) VALUES PER FILE
                               1=OFF WEAPONS
7600 C-
                               2=OFFENSIVE
7700 C-
7300 C-
                               3=NEUTRAL
                               4=DEFENSIVE
7900 C-
3000 C-
                               5=DEF FATAL
                               6=UTRADEOFF
3100 C-
3200 C- CONCO ARE THE CONVERSION COEFFICIENTS N(I) VALUES PER FILE
9300 C- PIPAIR ARE THE PAIRED PERF INDEX VALUES NPAIR(I) VALES PER PAIR
                                 PER FILE
3500 C- ISTATP ARE THE PAIRED STATE DATA SAME AS ISTATS BUT NO 6
8600 C- SECTIT A TITLE FOR SECTION, PARTIT-A TITLE FOR PAIRS
9700 DO 200 I=1,NFILES
3300 READ(2,/) N(I)
3900
      JK=N(I)/10
9000 KJ=JK+10
9100 READ(2,/) (PIS(I,J),J=1,N(I))
9200
      IF(KJ.EQ.N(I)) READ(2,300) BLANK
9300 READ(2,300) (SECTIT(I,J),J=1,70)
9400 READ(2,300) (SECTIT(I,J),J=71,140)
      READ(2,/) (ISTATS(I,J),J=1,N(I)) '.
READ(2,/) (CONCO(I,J),J=1,N(I))
9500
9600
9700 200 CONTINUE
9800 WRITE(1,310)
9900 310 FORMAT ("I JUST READ ALL THE SECTION DATA")
10000
       IF (ICALC.EQ.1.OR.ICALC.EQ.5) 60 TO 500
10100
       DO 400 I=1, NFILES
10200
       READ(3,/) MPAIR(I)
       READ(3,300) (PARTIT(I,J),J=1,70)
10300
       READ(3,/) (PIPAIR(I,J),J=1,NPAIR(I))
READ(3,/) (ISTATP(I,J),J=1,NPAIR(I))
10400
10500
10500
       400 CONTINUE
10700
       WRITE (1.320)
       320 FORMAT("I JUST READ PAIR A DATA")
10300
       DO 500 I=1.NFILES
11000
       K=I+NFILES
```

```
11100 READ(6./) MPAIR(K)
11300 READ(6,300) (PARTIT(K,J),J=1,70)
11300 READ(6,/) (PIPAIR(K,J),J=1,NPAIR(K))
       READ(6./) (ISTATP(K.J).J=1.NPAIR(K))
11400
11500 500 CONTINUE
11600 WRITE(1.330)
11700 330 FORMAT("I JUST READ PAIR B DATA")
11800 300 FORMAT(70A1) .
11900 WRITE(1,332)
12000 332 FORMAT ("DATA ARE IN")
12100 WRITE (IPRINT . 410)
12200 410 FORMAT (1H1,2X, "THE FOLLOWING DATA IS USED IN THIS RUN")
12300 WRITE (IPRINT. 300) ((SECTIT(I.J).J=1.140).I=1.NFILES)
13400 NBIG=0
12500
       MPBIG=0
12600 DO 501 I=1,NFILES
12700 IF (N(I).6T.NBIG) NBIG=N(I)
12800 IF(MPAIR(I).5T.MPBIG) MPBIG=MPAIR(I)
12900
       501 CONTINUE
13000 NPTS=200./DELTA+1
13100 C-
13200 C-
13300 C- SECTION INDEX FREQUENCY DISTRIBUTIONS IN TIME
13400 C-
13500 C-
13600 DO 600 I=1.NBIG.ICOMP
13700
       KSET=I
13800
       K=0
       DO 550 J=1.NFILES
13900
      IF(N(J).LT.I) 60 TO 550
K=K+1
14000
14100 K=K+1
14200 A(K)=PIS(J+I)
14300 KPIS(I)=K
14400 B(K)=CONCO(J+I)
14500 550 CONTINUE
      IF (K.LT.10) 60 TO 610
14600
14700 CALL FREDIS (-100., 100., DELTA, A, K, FREQ, CUMP, ANS)
14800 DO 570 J=1, NPTS
14900
       FPIS(I, J) = FREQ(J)
       FPIS(I, J) = REQ(J)

570 CUMPIS(I, J) = CUMP(J)

PISMN(I) = ANS(I)

PISDEV(I) = ANS(2)

PISM3(I) = ANS(3)
15000
15100 PISMN(I) =ANS(1)
15200 PISDEV(I) =ANS(2)
15300
15400 PISM4(I) =ANS(4)
15500 CALL FREDIS (-100., 100., DELTA, B, K, FREQ, CUMP, ANS)
15600 DO 580 J=1.NPTS
15700
       FCC(I.J) =FREQ(J)
15700 FCC(1-J)=REG(3)
15800 580 CUMPC(1-J)=CUMP(J)
15900 CCMN(I)=RNS(I)
14000 CCDEV(I)=RNS(S)
16100
       CCM3(1) =ANS(3)
16200 CCM4(I) =ANS(4)
16200 CCM4(I)=ANS(4)
16300 600 CQNTINUE
16400 50 TQ 550
15500 610 KSET=I-ICOMP
15600 620 CONTINUE
16700 WRITE(1:333) KSET
16800 333 FORMAT("I JUST FINISHED SECTION FREQ DATA FOR", 13, " PTS")
16900
       15 (10ALC.EQ.1.QR.10ALC.EQ.5) 60 TO 820
```

```
17000 C-
17100 C-
17200 C- CALCULATE PAIRED INFORMATION FREQUENCY DATA
17300 C-
17400 C-
17500 DO 800 I=1.NPBIG.ICOMP
17600 KPARLS=I
17700 K=0
17300 KQ=NFILES+2
17900 DO 650 J=1,KQ
13000 IF (NPAIR(J).LT.I) 60 TO 650
13100
       K=K+1
18200 A(K)=PIPAIR(J,I)
18300 KIPAIR(I)=K
13400 650 CONTINUE
13500 IF(K.LT.10) 60 TO 310
13600 CALL FREDIS (-100., 100., DELTA, A, K, FREQ, CUMP, ANS)
13700 DO 770 J=1,NPTS
18800 FPIP(I,J)=FREQ(J)
       770 CUMPIP(I,J)=CUMP(J)
PIPMN(I)=ANS(1)
13900
19000
19100 PIPDEV(I) =ANS(2)
19200 PIPM3(I) =ANS(3)
19300 PIPM4(I)=ANS(4)
19400 300 CONTINUE
19500 60 TO 920
19600 310 KPARLS=I-ICOMP
19700 320 CONTINUE
19300 WRITE(1,334) KPARLS
19900 334 FORMAT("I JUST FINISHED PAIRED FRED DATA FOR", 13, " PTS")
20000 C-
20100 C-
20200 C- CALCULATE SECTION MANEUVER CONVERSION DATA
50300 C-
20400 C-
20500 IF(ICALC.LT.3) 50 TO 1201
20500 DO 350 I=1,6
20700 DO 350 J=1,6
20300 CPS(I, J)=0.
20900 350 NCS(I,J)=0.
21000 DO 900 I=1.NFILES
21100 NN=N(I)-1
21200 DD 900 J=1,NN
21300 IF(ISTATS(I,J).LE.O.DR.ISTATS(I,J+1).LE.O) SD TD 900
21400 IF (ISTATS(I, J).E9. ISTATS(I, J+1)) 60 TO 900
21500 IDEX=ISTATS(I.J)
      JDEX=ISTATS(I, J+1)
21500
21700 MCS (IDEX, JDEX) =MCS (IDEX, JDEX) +1
21300 900 CONTINUE
21900 DO 1000 I=1.6
       TC(I) = 0.
55000
22100 DO 1000 J=1.5
22200 1000 TO(I) =NOS(I+J)+TO(I)
```

```
22300 DO 1200 I=1.6
22400 DD 1200 J=1,6
22500 IF(I.EQ.J) 5D TD 1200
22500 IF(FC(I).LT.0.5) CPS(I,J)=0.
22700 IF(TO(I).LT.0.5) 53 TG 1200
228800 CPS(I, J) = MCS(I, J) \rightarrow TC(I)
22900 1200 CONTINUE
23000 1201 CONTINUE
23100 WRITE(1:335)
33200 335 FORMAT("I JUST FINISHED SECTION MANEUVER CONV DATA")
23300 C-
23400 C-
33500 C- CALCULATE TIME IN STATE DISTRIBUTION
23600 0-
23700 C-
23300 IF (ICALC.LT.3) 60 TO 2702
23900 DO 1600 I=1.6
24000 IFL(I)=1
24100 DO 1600 J=1,300
24200 1600 ITIS(I,J)=0.
24300 DO 1300 I=1.NFILES
24400 NN=N(I)-1
24500 DO 1300 J=1,NN
24600 M=ISTATS(I,J)
24700 L=IFL(M)
24800 IF (ISTATS (I.J) .EQ. ISTATS (I.J+1)) 60 TO 1750
24900 IFL(M)=IFL(M)+1
25000 1750 ITIS(M,L)=ITIS(M,L)+1
25100 IF (J.EQ.NN.AND.ISTATS(I, J).EQ.ISTATS(I, J+1)> ITIS(M,L)=0.
25200
       IF (ITIS (M.L) .EQ. 0) IFL (M) = IFL (M) -1
25300
        1800 CONTINUE
25400
       TMAX=0.
25500 DO 2000 I=1,6
25600 NN=IFL(I)
25610
        TMAX=0.
25700 DO 1350 J=1,NN
25800 A(J)=ITIS(I+J)
25900 1350 IF(ITIS(I+J).ST.TMAX) TMAX=ITIS(I+J)
26000 IF(TMAX.LT.0.5) 60 TO 2050
26100 DEL=TMAX/50.
26200 DO 1900 K=1,51
36300 1900 TSCALE(I,K)=(K-1) ◆DEL
36310 IF(NN.LT.3) 60 TO 2050
36400 CALL FREDIS (0., TMAX, DEL, A, NN, FREQ, CUMP, ANS)
26500 DO 1950 K=1,51
26600
       TFREQ(I,K) =FREQ(K)
26700 1950 TCUMP(I,K) =CUMP(K)
26900 TMEAN(I) =ANS(1)
26900 TDEV(I) =ANS(2)
27000
        TMOM3 (1) =ANS (3)
27100 TMOM4 (1) =ANS (4)
27200 GO TO 2000
```

```
27300 2050 CONTINUE
27400 DO 2060 K=1,51
27500 TSCALE(I+K)=0.
27600 TFREQ(I,K)=0.
27700 2060 TCUMP(I,K)=0.
27300 TMEAN(I)=0.
27900 TDEV(I)=0.
28000 TMQM3(I)=0.
23100 TMQM4(I)=0.
33200 2000 CONTINUE
28300 WRITE(1,2001)
23400 2001 FORMAT("I JUST FINISHED SECTION TIME IN STATE")
29500 C-
29600 C-
23700 C- CALCULATE PAIRED MANEUVER CONVERSION DATA
23300 C-
23900 C-
29000 IF (ICALC.NE.4) 60 TO 2702
29100 DO 2100 I=1,5
29200 DO 2100 J=1.5
29300 CPP(I.J)=0.
29400 2100 NCP(I,J)=0
29500 NX=2. +NFILES
29600 DO 2200 I=1.NX
29700
       NN=NPAIR(I)-1
29800 DO 2200 J=1,NN
29900 IF(ISTATP(I,J).LE.O.DR.ISTATP(I,J+1).LE.O) 5D TD 2200
30000 IF(ISTATP(I,J).EQ.ISTATP(I,J+1)) 50 TO 2200
30100 IDEX=ISTATP(I,J)
30200 JDEX=ISTATP(I.J+1)
30300 NCP (IDEX, JDEX) = NCP (IDEX, JDEX) +1
30400 2200 CONTINUE
30500 DO 2300 I=1,5
30600 TC(I)=0.
30700 DO 2300 J=1,5
30900
       2300 TC(I)=TC(I)+NCP(I,J)
       DO 2400 I=1.5
31000 DO 2400 J=1,5
31100
      IF (I.EQ.J) 60 TO 2400
31200
       IF (TC(I).LT.0.5) CPP(I,J)=0.
      IF (TC (1) .LT. 0.5) 60 TO 2400
31300
31400 CPP(I+J)=NCP(I+J)/TC(I)
      2400 CONTINUE
31500
       WRITE (1,2401)
31600
31700 2401 FORMAT ("I JUST FINISHED PAIRED MAN CONV")
31800 C- C-
31900 C-
32000 C- CALCULATE TIME IN STATE FOR PAIRS
32100 C-
35500 C-
32300 DG 2500 I=1.5
32400 IFM(I)=1
32500 DO 2500 J=1.300
32600
      2500 ITIP(1. D=0
32700 DO 2600 I=1.HX
32900 MH=NPAIR(I)-1
```

```
32900 DO 2600 J=1.NM
33000
      M=ISTATP(I, J)
      L=IFM(M)
33100
33200 IF (ISTATP (I, J) .EQ. ISTATP (I, J+1)) 50 TO 2550
33300 IFM(M)=IFM(M)+1
33400
       2550 ITIP(M,L)=ITIP(M,L)+1
23500 IF (J.EQ.NH.AND.ISTATP(I, J).EQ.ISTATP(I, J+1)) ITIP(M,L)=0
33600
      IF (ITIP (M.L) . EQ. 0) IFM (M) = IFM (M) -1
33700
      2600 CONTINUE
33300
       TMAX=0.
      DG 2700 I=1.5
33900
34000 HN=IFM(I)
34100
      TMAX=0.
34200
       DO 2610 J=1.NN
34300 A(J)=ITIP(I,J)
34400 2610 IF(ITIP(I,J).GT.TMAX) TMAX=ITIP(I,J)
34500
      IF (TMAX.LT.0.5) 60 TO 2655
34600
       DEL=TMAX/50.
34700 DO 2620 K=1,51
34800 2620 TPCALE(I,K)=(K-1) *DEL
34810 IF (NN.LT.3) GO TO 2655
34900
       CALL FREDIS(0., TMAX, DEL, A, NN, FREQ, CUMP, ANS)
35000 DO 2650 K=1.51
35100
      TPFREQ(I,K)=FREQ(K)
35200 2650 TPCUMP(I.K)=CUMP(K)
35300
       TPMEAN (1) =ANS (1)
35400 TPDEV(I) =ANS(2)
      TPMOM3(I) =ANS(3)
TPMOM4(I) =ANS(4)
35500 TPMOM3(I) =ANS(3)
35600
       60 TO 2700
35700
35300 2655 CONTINUE
35900 DO 2656 K=1,51
36000 .TPFREQ(I,K)=0.
36100 TPCUMP(I,K)=0.
36200 2656 TPCALE(I,K)=0.
36300 TPMEAN(I)=0.
36400 TPDEV(I)=0.
36500 TPMOM3(I)=0.
36600 TPMOM4(I)=0.
36700 2700 CONTINUE
35900 2702 CONTINUE
35900 WRITE(1,2701)
37000 2701 FORMAT("I JUST FINISHED PAIRED TIME IN STATE-OUTPUT BESINS")
37010 C-
37020 C- BEGIN OUTPUT OF THE COMPUTED DATA
37030 C-
37040 C- THE COMPUTED DISTRIBUTION OF THE SECTION PERF INDICES
37050 C-
```

```
37100 DO 7950 J=1, NPTS
37200 7950 MXX(J) =-100.+(J-1) +DELTA
37300 WRITE (IPRINT, 8000)
37400 3000 FORMAT (1H1,2X, "PERFORMANCE INDICES DISTRIBUTION")
37500 NMXPT=NPTS/10
37600 NMXPT=NMXPT+10
37700 DO 9000 KQ=1,NMXPT,10
37900 KQ9=KQ+9
37900 WRITE(IPRINT,8001) (MXX(I),I=KQ,KQ9)
38000 8001 FORMAT(2x, "TIME FREQ(", 14, ") FREQ(", 14, ") FREQ(", 38100 - 14, ") FREQ(", 14, ")")
38300 DO 9000 J=1,KSET,ICOMP
33400 WRITE(IPRINT, 8950) J, (FPIS(J,K), K=KQ,KQ9)
38500 8950 FORMAT(2X,14,F12.5,9F12.5)
33600
       9000 CONTINUE
33700 NR=NMXPT+1
38800 WRITE (IPRINT, 8001) (MXX(I), I=NR, NPTS)
38900 DO 9001 J=1,KSET,ICOMP
       WRITE (IPRINT, 8950) J, (FPIS (J,K), K=NR, NPTS)
39000
39100 9001 CONTINUE
39200
       WRITE (IPRINT, 8975)
39300 8975 FORMAT (1H1,2X, "SUMMARY STATISTICS FOR PERF INDICES DIST")
39400
       WRITE (IPRINT, 9002)
39500 9002 FORMAT (2X, "TIME NPTS MEAN VARIANCE
39600 -"
             4THMOM")
39700 DO 9004 I=1,KSET,ICOMP
       WRITE (IPRINT, 9003) I, KPIS(I), PISMN(I), PISDEV(I), PISM3(I), PISM4(I)
39800
39900
       9004 CONTINUE
40000 9003 FORMAT (2X, 14, 17, F7. 2, F10. 2, F12. 2, F14. 2)
40100 DO 10000 J=1,KSET,IGRAF
       WRITE (4,9200) J
40200
       9200 FORMAT ("TIME ", 14)
40300
40400 BACKSPACE 4
       READ (4.9205) (NAME2(I), I=31,40)
40500
       9205 FORMAT (10A1)
40600
40700 DO 9500 K=1,NPTS
40800 B(K) = CUMPIS(J, K)
40900 9500 A(K)=FPIS(J,K)
       CALL PLOT (MXX, A, NPTS, IPRINT, NAME2, NAME1)
41000
41100
       IF (GRAFOP.EQ.-1) CALL PLOT (MXX, B, NPTS, IPRINT, NAME2, NAME3)
41200
       10000 CONTINUE
41300 WRITE(1,2999)
       2999 FORMAT (" PISECT IS OUT")
41400
41410 C-
41420 C- THE COMPUTED DISTRIBUTION OF THE CONVERSION COEFFICIENTS
41430 C-
41500
       WRITE (IPRINT, 3000)
       3000 FORMAT (1H1, 2X, "CONVERSION COEFFICIENT DISTRIBUTION")
41500
41700
       DO 3100 KO=1, NMXPT, 10
41800
       KQ9=KQ+9
41900
       WRITE (IPRINT, 8001) (MXX(I), I=KQ, KQ9)
```

```
42000 DO 3100 J=1.KSET.ICOMP
42100 WRITE (IPRINT, 8950) J. (FCC (J.K), K=KQ, KQ9)
43200 3100 CONTINUE
42300 WRITE (IPRINT, 8001) (MXX (I), I=NR, NPTS)
42400 DO 3101 J=1.KSET.ICOMP
       WRITE (IPRINT, 8950) J. (FCC (J.K), K=NR, NPTS)
42500
       3101 CONTINUE
42600
42700 WRITE (IPRINT, 3120)
       3120 FORMAT (1H1,2X, "SUMMARY STATISTICS FOR CONVERSION COEFF")
42900
42900
       WRITE (IPRINT, 9002)
43000 DO 3102 I=1.KSET.ICOMP
43100 WRITE(IPRINT, 9003) I.KPIS(I), COMM(I), CODEV(I), COM3(I), COM4(I)
       3102 CONTINUE
43200
       DO 3200 J=1.KSET.IGRAF
43300
43400 WRITE (4,9200) J
43500 BACKSPACE 4
43600 READ(4,9205) (NAME4(I), I=31,40)
43700
       DO 3150 K=1, NPTS
43800 B(K) = CUMPCC (J.K)
43900 3150 A(K)=FCC(J+K)
44000 CALL PLOT (MXX, A, NPTS, IPRINT, NAME4, NAME1)
44100
       IF (GRAFUP.EQ.-1) CALL PLUT (MXX, B, NPTS, IPRINT, NAME4, NAME3)
44200 3200 CONTINUE
44300 WRITE(1,3201)
       3201 FORMAT ("CONV COEFF IS OUT")
44400
44500 IF (ICALC.NE.1.AND. ICALC.NE.4) 60 TO 3603
44510 C-
44520 C- THE COMPUTED DISTRIBUTION OF THE PAIRED PERFORMANCE INDICES
44530 C-
44600
       WRITE (IPRINT, 3300)
44700 3300 FORMAT (1H1, 2X, "PAIRED PERFORMANCE INDICES DISTRIBUTION")
44800 DO 3400 KQ=1,NMXPT,10
44900
       KQ9=KQ+9
45000
       WRITE (IPRINT, 8001) (MXX(I), I=KQ, KQ9)
45100 DO 3400 J=1, KPARLS, ICOMP
45200 WRITE (IPRINT, 8950) J, (FPIP (J, K), K=KQ, KQ9)
45300
       3400 CONTINUE
45400
       WRITE (IPRINT, 8001) (MXX(I), I=NR, NPTS)
45500 DO 3401 J=1, KPARLS, ICOMP
45600 WRITE (IPRINT, 8950) J. (FPIP (J.K) K=NR, NPTS)
45700 3401 CONTINUE
45800 WRITE (IPRINT, 9002)
45900 DO 3402 I=1, KPARLS, ICOMP
45000 - WRITE(IPRINT,9003) I, KIPAIR(I), PIPMN(I), PIPDEV(I), PIPM3(I),
46100 -PIPM4(I)
45200
       3402 CONTINUE
45300 DO 3600 J=1.KPARLS.IGRAF
46400 WRITE(4,9200) J
46500 BACKSPACE 4
46500 READ(4,9205) (NAME2(I),I=31,40)
46700 DO 3550 K=1.NPTS
45500 B(K)=CUMPIP(J.K)
45900 3550 A(K)=FPIP(J+K)
```

```
47000 CALL PLOT (MXX+A+NPTS+IPRINT+NAME2+NAME1)
       IF (GRAFOP.E0.-1) CALL PLOT (MXX, B, NPTS, IPRINT, NAME2, NAME3)
47100
47200
        3600 CONTINUE
47300
        3603 CONTINUE
47400
        WRITE(1,3601)
       3601 FORMAT ("PI PAIR IS OUT")
47500
       IF (ICALC.LT.3) 60 TO 3683
47600
47700
        WRITE (IPRINT, 3604)
47800 3604 FORMAT (1H1, 2X, "SECTION MANEUVER CONVERSION/CONVERSION",
47900 -" PROBABILITY MATRIX")
48000 WRITE (IPRINT, 3608)
48100 3608 FORMAT(15X, "OFF WEP OFFENSIVE NEUTRAL DEFENSIVE ",
48200 -"DEF FAT TRADEOFF")
43300 WRITE (IPRINT, 3610) (CPS (1, J), J=2,6)
43400
        3610 FORMAT (2X) "OFF WEP
                                        +",5X,5F10.4)
       WRITE (IPRINT, 3612) CPS (2,1), (CPS (2, J), J=3,6)
43500
        3612 FORMAT (2X, "OFFENSIVE ", F10.4, 4X, "+", 5X, 4F10.4)
48600
       WRITE(IPRINT.3614) (CPS(3,J),J=1,2),(CPS(3,J),J=4,6)
3614 FORMAT(2X,"NEUTRAL . ",2F10.4,4X,"+",5X,3F10.4)
43700
43300
43900
        WRITE(IPRINT, 3616) (CPS(4, J), J=1, 3), (CPS(4, J), J=5,6)
        3616 FORMAT (2X, "DEFENSIVE ", 3F10.4, 4X, "+", 5X, 2F10.4)
49000
       WRITE(IPRINT,3618) (CPS(5,J),J=1,4),CPS(5,6)
3618 FORMAT(2X,"DEF FAT ",4F10.4,4X,"*,"5X,F10.4)
49100
49200
49300
        WRITE (IPRINT, 3620) (CPS (6, J), J=1,5)
        3620 FORMAT (2X, "TRADEOFF ", 5F10.4, 4X, "+")
49400
       WRITE (IPRINT, 3622)
49500
        3622 FORMAT (1H1, 2X, "SECTION TIME IN STATE DISTRIBUTION")
49600
49700 WRITE (IPRINT, 3624)
       3624 FORMAT (8X, "TIME FREQ (OFFWEP) TIME FREQ (OFFNSV)"
49800
49900 -" TIME FREQ(NEUTRL) TIME FREQ(DEFNSV) TIME FREQ(DEFFAT)", 50000 -" TIME FREQ(TRADE ) ")
30100 DO 3650 J=1,51
       WRITE (IPRINT, 3626) ((TSCALE (I, J), TFREQ (I, J)), I=1,6)
50200
50300
        3626 FORMAT (2X,6(F10.2,F10.4))
50400
        3650 CONTINUE
50500
        WRITE (IPRINT, 3628)
       3628 FORMAT (1H1,4X, "SUMMARY STATISTICS FOR SECTION MANEUVER ...
50600
           CONV"
50700 WRITE (IPRINT, 3630)
50800 3630 FORMAT (2X."STATE
                                    MEAN
                                                VARIANCE"
50810 -,"
                                       NPTS")
          3RDMDM
                          4THMOM
50900 WRITE (4,3655)
        3655 FORMAT ("OFF WEP"/"OFFENSIVE"/"NEUTRAL"/"DEFENSIVE"/"DEF
51000
             FAT"
51100 -"TRADE OFF")
51200
       DO 3654 J=1.6
        3654 BACKSPACE 4
51300
51400 DO 3660 J=1.6
51500 READ(4,3657) ANNA,KING
51600
        3657 FORMAT (285)
51700 WRITE(IPRINT,3662) ANNA,KING,TMEAN(J),TDEV(J),TMOM3(J),TMOM4(J)
51710 -, IFL (J)
51800 3662 FORMAT (2X, 2A5, 4F10.2, 17)
51900
        3660 CONTINUE
52000 DO 3665 J=1.6
52100 3665 BACKSPACE 4
```

```
52200 DO 3680 I=1.6
52300 DO 3670 J=1.51
53400 A(J)=TFREQ(I+J)
52500 3670 B(J) =TSCALE(I, J)
52600 READ(4,3656) (NAME5(K),K=31,40)
52700 3656 FORMAT(10A1)
32800 CALL PLOT (B.A.51. IPRINT, NAMES, NAME1)
52900 IF(GRAFOP.NE.-1) GO TO 3680
53000 DO 3675 J=1.51
53100 3675 A(J)=TCUMP(I,J)
53200 CALL PLOT (B.A.51, IPRINT, NAMES, NAMES)
53300 3680 CONTINUE
53400
       3683 CONTINUE
53500 WRITE(1,3681)
53600
      3681 FORMAT ("SECT MN CNV IS OUT")
53700
      IF (ICALC.NE.4) 60 TO 3800
53800
       WRITE (IPRINT, 3682)
53900 3682 FORMAT(1H1,2X,"PAIRED MANEUVER CONVERSION PROBABILITY",
54000 -" MATRIX")
54100 WRITE (IPRINT, 3608)
54200
       WRITE (IPRINT, 3610) (CPP (1, J), J=2,5)
      WRITE (IPRINT, 3612) CPP (2,1), (CPP (2, J), J=3,5)
54300
      WRITE (IPRINT, 3614) (CPP (3, J), J=1,2), (CPP (3, J), J=4,5)
54400
54500
       WRITE (IPRINT, 3616) (CPP (4, J), J=1,3), (CPP (4, J), J=5,5)
       WRITE (IPRINT, 3618) (CPP (5, J), J=1,4)
54600
54700 WRITE (IPRINT, 3684)
      3684 FORMAT (1H1, 2X"PAIRED TIME IN STATE DISTRIBUTIONS")
54800
54900 WRITE (IPRINT, 3624)
      DO 3686 J=1,51
55000
       WRITE (IPRINT, 3626) ((TPCALE (I, J), TPFREQ (I, J)), I=1,5)
55100
55200
      3686 CONTINUE
55210
      WRITE (IPRINT, 3687)
55300
      WRITE (IPRINT, 3630)
55400 WRITE (4, 3655)
55500 DO 3689 J=1,6
55600 3689 BACKSPACE 4
       3697 FORMAT (1H1, 2X, "SUMMARY STATISTICS FOR PAIRED TIME IN STATE")
55800
56000 DO 3690 J=1.5
56100 READ(4,3657) ANNA,KING
56200 WRITE(IPRINT,3662) ANNA,KING,TPMEAN(J),TPDEV(J),TPMOM3(J)
56300 -, TPMOM4(J), IFM(J)
56400 3690 CONTINUE
56500 DO 3691 J=1.5
56600 3691 BACKSPACE 4
```

```
56700 DO 3698 I≈1,5
56800 DO 3698 J≈1,51
56900 A(J) = TPFREQ(I+J)
57000
       3692 B(J) = TPCALE(I.J)
57100 READ(4,3656) (NAME5(K),K=31,40)
57200 CALL PLOT (B.A.51. IPRINT, NAMES, NAME1)
57300 IF (GRAFOP.NE.-1) 60 TO 3698
57400 DO 3694 J≈1,51
57500
       3694 A(J)≈TPCUMP(I,J)
57600 CALL PLOT (B.A.51. IPPINT. NAMES. NAMES)
57700
      3698 CONTINUE
57800
       3800 CONTINUE
57900
       WRITE (1,3699)
53000 3699 FORMAT("ALL DATA ARE OUT")
59100 C-
58200 C- START OUTPUT OF EXPECTED PATHS
58300 C-
53310 DO 4005 I=1.101
53320 A(I)=BLANK
58330
      4005 B(1)=BLANK
59400
       DO 4000 J=1,101,10
58500 B(J)=PLUS
       A(J) =DOT
53600
58700
       4000 CONTINUE
58300
       WRITE (IPRINT, 4001)
58900 4001 FORMAT (1H1,2X, "EXPECTED PATHS FOR CONTINUOUS DATA"///
59000 -10X, " • PERFORMANCE INDEX SECTION"/
59100 -10X," + PERFORMANCE INDEX PAIRS"/
59200 -10X+" & CONVERSION COEFFICIENT SECTION"/
59300 -//8X,"-100
59310 -"0 +20
                       -30
+40
                                  -60 -40 -20
+60 +80 +
59400 WRITE (IPRINT, 4002) (B(J), J=1, 101), (A(J), J=1, 101)
59500
       4002 FORMAT (2X, "TIME", 4X, 101A1/2X, "SECS", 4X, 101A1)
       DO 4100 J=1,101
59600
59700
       4100 B(J)=PLUS
       WRITE (IPRINT, 4101) (B(J), J=1,101)
59800
59900
       4101 FORMAT (10X, 101A1)
      IF (ICALC.EQ. 1. OR. ICALC.EQ. 5) KPARLS=KSET
59910
      DO 5000 J=1, KPARLS, ICOMP
60000
       DO 4003 I=1,101
50100
60200
       4003 A(I)=BLANK
       A(51) = DOT
60300
60400
       A(1) =PLUS
60500
       A(101) =PLUS
60600
       IF (J. ST. KSET) 60 TO 4004
       K=0.50+CCMN(J)+50.5
50700
       IF (K.GE.1.AND.K.LE.101) A(K) = DOLL
60800
60900
       L=0.50+PISMN(J)+50.5
61000
       IF (L.GE.1.AND.L.LE.101) A(L)=STAR
       4004 M=0.50+PIPMN(J)+50.5
61100
       IF (M. GE. 1. AND. M. LE. 101) A (M) =PLUS
61200
61300
       WRITE (IPRINT, 4006) J. (A(KK), KK=1,101)
61400
       4006 FORMAT (3X, 14, 3X, 101A1)
61500
       5000 CONTINUE
61600
       CALL EXIT
51700
       END
```

```
51800 SUBROUTINE FREDIS (ALPHA, BETA, DELTA, X, NDATA, FREQ, CUMP, ANS)
61310 C-
61820 C- THIS SUBROUTINE USES FREQUENCY DISTRIBUTION
61830 C-
          RECOVERY TECHNIQUE--- ** PER ULTRASYSTEMS RPT
61946 C-
61850 C- IT CALLS AN INTEGRATION SUBROUTINE (QSF) AND A MOMENTY
           < CALCULATION
61860 C- SUBROUTINE (MOMEN)
61370 C-
-1880 C- THE DISTRIBUTION FUNCTION OF THE X STRING VECTOR IS COMPUTED
61881 C- AND PLACED IN FRED AFTER IT IS NORMALIZED
51893 C- X HAS HDATA VALUES WITH A MAXIMUM OF BETA (RANGE VALUE)
51884 C- A MINIMUM OF ALPHA (RANGE VALUE) TO BE COMPUTED OVER
61935 C- A GRID VALUE OF DELTA
61886 C-
61987 C- THE PROGRAM ALSO RETURNS THE NORMALIZED CUMULATIVE PROBABILITY
61888 C-
           OF OCCURENCE (CUMP) AND THE FIRST FOUR MOMENTS (ANS)
61889 C-
61900 DIMENSION
          UBD (5) , ANS (4) , X (500) , FREQ (500) , CUMP (500) , Y (500) , XI (500) ,
62000 -FHAT (500) +U (500)
62100 DIMENSION NX (500) - RF (500)
62200 UBO(1) =ALPHA
62300 UBD(2)=BETA
62400 UBO(3)=DELTA
62500 SUM1=0.
62600 SUM2=0.
62700 NPTS=(BETA-ALPHA) / DELTA+1
62800
      SUMAIJ=0.
62900 NINT=(BETA-ALPHA)/DELTA
53000 DD 10 I=1.NDATA
53000 DO 10 I=1.NDATA
63100 DO 10 J=1.NDATA
UAMMS+S++((L)X-(I)X)=LIAMMS 01 00566
63300 XMU=0.
63400 XMU=SUMAIJ
       XMU=XMU/(NDATA+(NDATA-1))
53500
63600 IF (ABS (XMU) .LT.1.E-08) RHO=0.
63700 IF (ABS (XMU) .LT.1.E-03) 50 TO 22
63800 IF (XMU.GT.1.) DELTA1=0.010
63900
       IF (XMU. GT. 1.) RHG= (DELTA1+ALOG (NDATA)+ALOG (XMU))/XMU
       IF (XMU.LE.1.) DELTA1=0.250
64000
64100 IF (XMU.LE.1.) RHO=DELTA1+ALOG (NDATA) /XMU.
64200 22 CONTINUE
64300 BINV=0.
64400 DO 30 I=1.NDATA
64500 ' DO 30 J=1.NDATA
64500 ECH=EXP(-1. +RH0+(X(I)-X(J))++2)
       FUNC= (X(I)-X(J)) ++2+ECH
54800 30 BINV=BINV+FUNC
64900 IF (ABS (BINV) .LT.1.E-08) B=0.
55000 IF (ABS (BINV) .LT.1.E-08) 60 TO 32
65100 BINV=BINV/(NDATA+(NDATA-1))
65200 B=1./BINV
55300 32 CONTINUE
```

```
65400 DO 40 I=1, NPTS
55500 40 Y(I) = ALPHA+(I-1) +DELTA
65600 DO 50 I=1.MPTS
65700 FHAT(I)=0.
55800 DO 50 J=1, NDATA
65900 STEP1=Y(I)-X(J)
66000 STEP2=EXP(-1*(B*STEP1)**2/2.)
66100 50 FHAT(I)=FHAT(I)+B/NDATA+STEP2
66200 CALL QSF(DELTA, FHAT, XI, NPTS)
66300 DO 500 J=1.NPTS
66400 IF (ABS (XI (NPTS)).5T.1.E-08) 60 TO 490
66500 FREQ(J)=0.
65600 CUMP (J) = 0.
66700 GO TO 500
66800 490 FREQ(J) = FHAT(J) / XI(NPTS)
66900 CUMP (J) =XI (J) /XI (MPTS)
67000 500 CONTINUE
67100 CALL MOMEN (FREQ, UBO, NPTS, ANS)
57200 RETURN
67300
       END
```

```
67400 SUBROUTINE OSF (H.Y.Z. NDIM)
57410 C- THIS IS A GENERAL INTEGRATION ROUTINE FOR EQUALLY SPACED
67480 C- FUNCTIONS (Y)
57430 C-
57440 C- THE SPACING OF Y IS H--- THE NUMBER OF POINTS IS NOIM
67450 C- THE INTEGRAL OF Y IS 2
67470 C- THE SUBPOUTINE USES A COMBINATION OF SIMPSONS RULE
67480 C- AND NEWTONS THREE-EIGHTHS RULE
67490, C-
67500 DIMENSION Y (1) . Z (1)
57600 HT=H+1./3.
57700 1 SUM1=Y(2)+Y(2)
57800 SUM1=SUM1+SUM1
67900 SUM1=HT+(Y(1)+SUM1+Y(3))
68000 AUX1=Y(4)+Y(4)
68100 AUX1=AUX1+AUX1
68200 AUX1=SUM1+HT+(Y(3)+AUX1+Y(5))
63300 AUX2=HT+(Y(1)+3.875+(Y(2)+Y(5))+2.625+(Y(3)+Y(4))+Y(6))
68400 SUM2=Y(5)+Y(5)
63500 SUM2=SUM2+SUM2
63600 SUM2=AUX2-HT+(Y(4)+SUM2+Y(6))
68700 Z(1)=0.
68800 AUX=Y(3)+Y(3)
63900 AUX=AUX+AUX
59000 Z(2)=SUM2-HT+(Y(2)+AUX+Y(4))
69100 Z(3)=SUM1
69200 Z(4)=SUM2
69300 IF (NDIM-6) 5,5,2
69400 2 DO 4 I=7,NDIM,2
69500 SUM1=AUX1
59600 SUM2=AUX2
69700 AUX1=Y(I-1)+Y(I-1)
69800
       AUX1=AUX1+AUX1
69900 AUX1=SUM1+HT+(Y(I-1)+AUX1+Y(I))
70000 Z(I-2)=SUM1
70100 IF(I-NDIM)3,6,6
70200 3 AUX2=Y(I)+Y(I)
70300 AUX2≈AUX2+AUX2
70400 AUX2=SUM2+HT+(Y(I-1)+AUX2+Y(I+1))
70500 4 Z(I-1)=SUM2
70600 5 Z(NDIM-1)=AUX1
70700 Z(NDIM) =AUX2
70300 RETURN
70900 6 Z(NDIM-1)=SUM2
71000
       Z (NDIM) = AUX1
71100 RETURN
71200 END
```

```
71300 SUBROUTINE MOMEN (F, UBO, NPTS, ANS)
71310 C-
71320 CHITHIS ROUTINE CALCULATES THE CLASSICAL MOMENTS OF A GIVEN
71330 C- FREQUENCY FUNCTION (F) HAVING A MAX (UBO(2)) A MIN (UBO(1))
71340 C- AND A GRID SIZE (UBD (3)) THE MOMENTS ARE PLACED IN ANS
71360 C- THE FIRST MOMENT (MEAN IS ABOUT THE ORIGIN
71370 C- ALL SUBSEQUENT MOMENTS ARE ABOUT THE MEAN
71380 C-
71400 - DIMENSION F (1) ANS (1) XM (500) Y (500)
71500
         DIMENSION UBO (3)
71800 TU HNS(I)=0.

71800 DD 20 I=1,NPTS

71900 Y(I)=UBD(1)+(I-1)+UBD(3)

72000 20 XM(I)=Y(I)+F(I)

72100 CALL OSE(UBD(2) VIII
71600 DO 10 I=1,4
72000 20 XM(I)=Y(I) +F(I)
72100 CALL QSF(UBQ(3), XM, XM, NPTS)
72200 ANS(I)=XM(NPTS)
72300 DQ 30 I=1, NPTS
72400 30 XM(I)=F(I) +(Y(I) -ANS(I)) ++2
        DO 30 I=1,NPTS
30 XM(I)=F(I) + (Y(I) - ANS(I)) ++2
CALL QSF(UBO(3),XM,XM,NPTS)
72500
72600
         ANS (2) =XM (NPTS)
72700 DO 40 I=1.NPTS
72700 DO 40 I=1,NPTS
72800 40 XM(I)=F(I)+(Y(I)-RNS(1))++3
72900 CALL QSF(UBO(3),XM,XM,NPTS)
73000 ANS(3)=XM(NPTS)
73100
        DO 50 I=1.NPTS
         50 XM(I)=F(I)+(Y(I)-ANS(1))++4
73200
        CALL QSF(UBD(3),XM,XM,NPTS)
ANS(4)=XM(NPTS)
73400
73500
        RETURN
73600 END
```

998 CONTINUE

77700

```
73700 SUBROUTINE PLOT (X.Y. NDATA, IPRINT, NAMEX, NAMEY)
73710 C-
73720 C- THIS ROUTINE PLOTS A GENERAL VECTOR Y VERSUS A GENERAL
73730 C- VECTOR X CONSISTING OF NOATA VALUES NOT NECESSARILY ORDERED
73750 C- NAMEX IS A 40 CHARACTER IDENTIFIER OF THE X VER(ALPHANUM)
73770 C-
73780 C- IPRINT IS THE OUTPUT LOGICAL UNIT NUMBER
73790 C-
73791 C- THE ROUTINE COMPUTES ITS DWN SCALE VALUES AND DEVELOPES
73792 C- ITS OWN OUTPUT---IT RETURNS NOTHING TO THE MAIN PROGRAM
73793 C-
73800 DIMENSION NAMEX (16) , NAMEY (16)
73900
       DIMENSION X(51),Y(51),PLOTS(51,51),Z1(51),Z2(51)
       DATA BLANK, STAR, XXX, PLUS/" ", "+", "X", "+"/
74000
      DATA DOT/"."/
74100
      DATA DASH/"-"/
74200
74300
      DO 10 J=1.51
74400 DD 10 K=1,51
      10 PLOTS (J.K) = BLANK .
74500
74600 DO 11 K=1,51
       11 PLOTS (51.K) = DOT
74700
      DO 121 J=1,51
74800
       121 PLOTS (J. 51) = DOT
74900
75000
      DO 131 J=1,51,5
      DO 131 K=1,51,5
75100
75200
      IF (J.EQ.51. GR.K.EQ.51) 60 TO 130
      60 TO 131
75300
      130 PLOTS (J.K) = DASH
75400
75500
      PLOTS (K. J) = DASH
      131 CONTINUE
75600
75700 XBIG=-9.9E06
75800 XSMALL=9.9E06
75900 YBIG=-9.9E06
76000
      YSMALL=9.9E06
76100 DO 999 I=1.NDATA
76200 IF (X(I).GT.XBIG.AND.Y(I).GT.(1.E-06)) XBIG=X(I)
      IF (X(I).ET.XSMALL.AND.Y(I).GT.(1.E-06)) XSMALL=X(I)
76300
       IF (Y(I).GT.YBIG) YBIG=Y(I)
75400
      IF (Y(I).LT.YSMALL) YSMALL=Y(I)
75500
76600
      999 CONTINUE
76700
      YDEL=YBIG-YSMALL
      XDEL=XBIG-XSMALL
75300
75900 IF (XDEL.LT.1.E-03.GR.YDEL.LT.1.E-03) RETURN
77000 TEST=1.E-07
77100
      DO 998 I=1,14
77200
       TEST=TEST+10.
77300
      DO 998 J=1.9
77400
       IF (YDEL.GT. (J+TEST).AND.YDEL.LE. ((J+1) +TEST)) YDEL=(J+1) +TEST
77500
       IF (XDEL.GT. (J+TEST).AND.XDEL.LE. ((J+1)+TEST)) XDEL=(J+1)+TEST
77600
      CONTINUE
```

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```
77800 XAV6=(XBIG+XSMALL)/2.
77900 YAVG=(YBIG+YSMALL)/2.
73000
       XMIN=XAVG-XDEL/2.
73100
      XM9X=XAV6+XDEL/2.
79200 YMIN=YAVG-YDEL/2.
73300 YMAX=YAVG+YDEL/2.
73400
       XING=(XMAX-XMIN)/50.
73500 YINC=(YMAX-YMIN)/50.
78600 DO 20 I=1.NDATA
73700
      IF (X(I).6T.XMAX) 60 TO 12
79800
      IF (X (D).LT.XMIN) 60 TO 13
73900 IF(Y(I).GT.YMAX) GO TO 16
79000 IF(Y(I).LT.YMIN) GO TO 17
79100 \cdot K = (X(I) - XMIN) + (1.2XINC) + 1.
79200 L=(Y(I)-YMIN)+(1.2YINC)+1.
79300 PLOTS(L+K)=STAR
79400
      60 TO 20
79500 12 K=51
79500 IF (Y(I).LT.YMIN) L=1
79700 IF(Y(I).GT.YMAX) L=51
79800 IF (Y(I).LT.YMIN.OR.Y(I).GT.YMAX) GO TO 19
79900 L=(Y(I)-YMIN)+(1.2YINC)+1.
      GO TO 19
30000
      13 K=1
30100
      IF (Y(I).LT.YMIN) L=1
80200
      IF (Y(I).GT.YMAX) L=51
30300
30400
      IF(Y(I).LT.YMIN.OR.Y(I).GT.YMAX) 60 TO 19
80500
      L=(Y(I)-YMIN)+(1.7YINC)+1.
30600
      60 TO 19
      16 L=51
30700
30800
      K=(X(I)-XMIN)+(1.7XINC)+1.
50900
      60 TO 19
31000 17 L=1
31100
      K = (X(I) - XMIN) + (1.7XINC) + 1.
31200
      19 PLOTS(L,K)=XXX
31300
      20 CONTINUE
31400
      DO 22 I=1,51
31500
       Z1(I) = XMIN+(I-1) + XINC
31600
      Z2(I) = YMIN+(I-1) + YINC
      SS CONTINUE
31700
      WRITE (IPRINT, 25)
31800
      25 FORMAT (1H1+//)
31900
82000 DO 30 K=1.51
32100 I=52-K
32200 WRITE (IPRINT-26) Z2(I) - (PLOTS(I, J) - J=1-51)
92300 26 FORMAT(2X,F10.4." + ",5141)
22400 30 CONTINUE
```

```
32500 WRITE (IPRINT, 40)
        40 FORMAT (15%, "+++++++++++++++++++++++++++++
            ("++++/
32700
        WRITE (IPRINT, 50)
33300
        50 FORMAT (16X,"+
82900
        WRITE (IPRINT, 45) Z1 (1), Z1 (11), Z1 (21), Z1 (31), Z1 (41), Z1 (51)
        45 FORMAT (9X,6F10.2)
83000
        WRITE (IPRINT, 46) (NAMEX (I) , I=1, 40) , (NAMEY (I) , I=1, 40)
33100
        46 FORMAT(10X, "THE X VARIABLE IS ",40A1/
10X, "THE Y VARIABLE IS ",40A1)
83200
83300 -
83400 RETURN
93500
        END
```

END QUIKLST 14.0 SEC.

TERMINOLOGY

ACM	- Acronym for Air Combat Maneuvering	
ACM State	- A descriptor of the ACM situation as offensive, defensive, etc.	
AIS	- Airborne Instrumentation Subsystem	
Bimodal	- Having two characteristic peaks.	
Bogie	- A term applied to the opposition aircraft in an engagement.	
Bogie Switching	- A maneuver wherin the opposition aircraft switches his offensive press to avoid being "predictable".	
Conversion Coefficient	An analysis term computed by combining the performance index and maneuver conversion computations.	
Conversion Probability	- The probability of converting from one ACM state to another.	
Coordination Consistency	- The difference between unity and the standard deviation of the section coordination term.	
Defensive	- A mathematical state where the subject aircraft or section is being threatened.	
Distributions	- A mathematical term applied to the probable range of events and how test data covers that range.	
Dominance	- A term applied when one aircraft or section is in decisive control of the engagement.	
Expected Path	- The locus of expected values of a variable.	
Fatal Defensive	- A mathematical state where the subject aircraft or section is in a weapons opportunity of an opponent.	
"Flash Through"	- A mathematical term indicating a transient situation (extreme short duration).	
Frequency Distribution	- A distribution of the frequency of occurrence of a variable as a function of the variable.	
Magnitude Sum	- A method of combining paired data to yield section data.	
Markov	- A mathematical term referring to a time independence occurrence of events.	

Multimodal	- Having several characteristic peaks.
Maneuver Conversion Model	- An ACM analysis model made up of ACM states.
Neutral	- A mathematical state where the subject aircraft has neither an advantage nor disadvantage.
Offensive	- A mathematical state where the subject aircraft is threatening an opponent.
Offensive Weapons	- A mathematical state where the subject aircraft has a weapons opportunity on an opponent aircraft.
Paired Data	- A term applied to data generated for a specific fighter-to-target pair.
Paired Coefficient	- An analysis parameter generated for a specific fighter-to-target pair.
Performance Index	 A time variant figure-of-merit which scales the offensive value of a fighter-to-target pair or aircraft section via the product of angle, range, and energy penalty functions.
Section Data	- A term applied to data generated for a fighter or target section.
Section Coefficient	- An analysis parameter for a fighter or target section.
Section Coordination	- An analysis parameter which accounts for the relative contribution of each aircraft in the section.
Semi-Markov	- A Markov process modified to include a time dependence only within a given state.
Significance Level	 A mathematical term representing a minimum accept- able tactical advantage or maximum acceptable disad- vantage.
State	- See ACM State.
Stochastic	- A mathematical term applied to a time dependent occurrence of events that are statistical in nature.
"Survival Sting"	- A term applied to a shortened tracking solution due to the tactical press of an opponent.
Target Aircraft	- An opponent aircraft; a bogie.

Trade Off

 An ACM state where, in a section, the offensive weapons and defensive fatal states exist simultaneously.

Trade Off Ratio

- The ratio of opponent aircraft shot down to friendly aircraft lost.

Trimodal

- Having three characteristic peaks.

Vector Sum

- A method of combining paired information.

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